

## TRAFFIC IMPACT ASSESSMENT

# PROPOSED REZONING AND SUBDIVISION: REMAINDER OF ERF 2833 GREAT BRAK RIVER, MOSSEL BAY

Report Number 23-041\_TIA



Date: January 2024

Revision (2)

## COVER LETTER

It is herewith certified that this Traffic Impact Investigation has been prepared according to requirements of the TMH 16 (Committee Draft 2.0 – May 2018) South African Traffic Impact and Site Traffic Assessment Manual.

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# QUALITY ASSURANCE DATA

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(on behalf of Urban Engineering (Pty) Ltd)

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## LIST OF ABBREVIATIONS

|        |   |
|--------|---|
| TIA    | Traffic Impact Assessment                       |
| SANRAL | South African National Roads Agency SOC Limited |
| RNIS   | Road Networks Information System                |
| PGWC   | Provincial Government of the Western Cape       |
| AMP    | Access Management Plan                          |
| AMG    | Access Management Guidelines (2016)             |
| RAG    | Road Access Guidelines (2002)                   |
| RDE    | Roadside Development Environment                |
| GLA    | Gross Leasable Area                             |
| SATGRM | South African Trip Generation Rates Manual      |
| LOS    | Level of Service                                |
| DoT    | Department of Transport                         |
| RDE    | Roadside Development Environment                |
| MR     | Main Road                                       |
| DR     | Divisional Road                                 |
| RNIS   | Road Network Information System                 |
| GRZ1   | General Residential Zone 1                      |
| SRZ1   | Single Residential Zone 1                       |
| BZIII  | Business Zone 3                                 |

## 1 INTRODUCTION

Urban Engineering (Pty) Ltd was appointed by New Care Innovations (Pty) Ltd to undertake a Transportation Investigation pertaining to the proposed rezoning and subdivision of Remainder Erf 2833, Great Brak River in Mossel Bay, Western Cape.

### 1.1 PROJECT BENEFIT AND CONTEXT

New Care Innovations (Pty) Ltd want to rezone and subdivide REM 2833, Great Brak River in Mossel Bay to create a residential development with Residential zoned erven. This is to satisfy the demand / opportunity that the client has recognized for this type of development in the Great Brak River area.

### 1.2 TERMS OF REFERENCE

Transportation investigations essentially need to be undertaken in accordance with the following guidelines:

- National Land Transport Act, 2009 (Government Gazette No. 32110)
- South African Traffic Impact & Site Traffic Assessment Manual (TMH 16 Volume 1, COTO)
- Access Management Guidelines (WCG Dept. Transport and Public Works, 2020)
- Manual for Traffic Impact Studies RR 93/635 (DoT, 1995)

To better align with the recommendations of the TMH16, the Access Management Guidelines recommends that when a development is likely to generate a minimum of 50 additional vehicular trips in a highest hour of its traffic generation, (including passer-by trips) a TIA is required.

### 1.3 PRIMARY OBJECTIVES OF THIS REPORT

This study will look at the effect of the additional traffic generated by the proposed operation on the surrounding road network. Where necessary, the report will aim to introduce mitigation measures to reduce this impact at the site, as well as on the surrounding transportation network.

### 1.4 STUDY OBJECTIVES

The study objectives are:

- i. Assess the traffic conditions on the existing road network.
- ii. Assess the traffic generation effects of the proposal (if any)
- iii. Assess the interface conditions between the road network and the proposed development
- iv. Highlight any traffic concerns resulting from the proposed development (including parking and non-motorised transport)
- v. Make recommendations.

### 1.5 SITE INVESTIGATION

The site was visited by Frans van Aardt of Urban Engineering (Pty) Ltd on 23 May 2023. Relevant measures and inspections were taken during the site visit. A record of some of the photos taken during the site visit has been attached as **ANNEXURE A** to this report.

## 2 LOCALITY

RE2833 is approximately 6ha in extent. The site is situated north of National Road 2 (N2) along Provincial road DR1583 (Sandhoogte). Access to the site is via DR1583. The site centre has approximate WGS 84 coordinates of 34° 3'17.88"S and 22°12'10.22"E. A basic locality plan has been included as Figure 2-1.

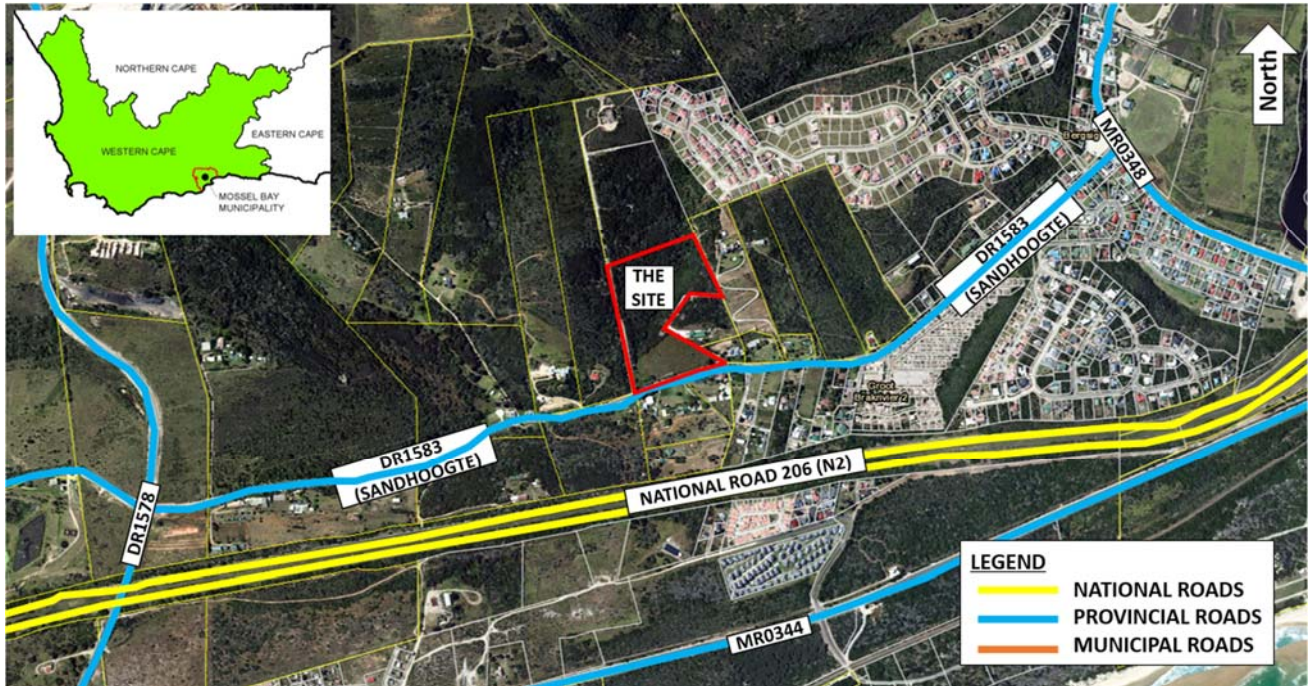


Figure 2-1 - Basic Locality Plan

## 3 STATUS QUO

RE2833 is currently undeveloped and covered in vegetation as indicated in the photo below.

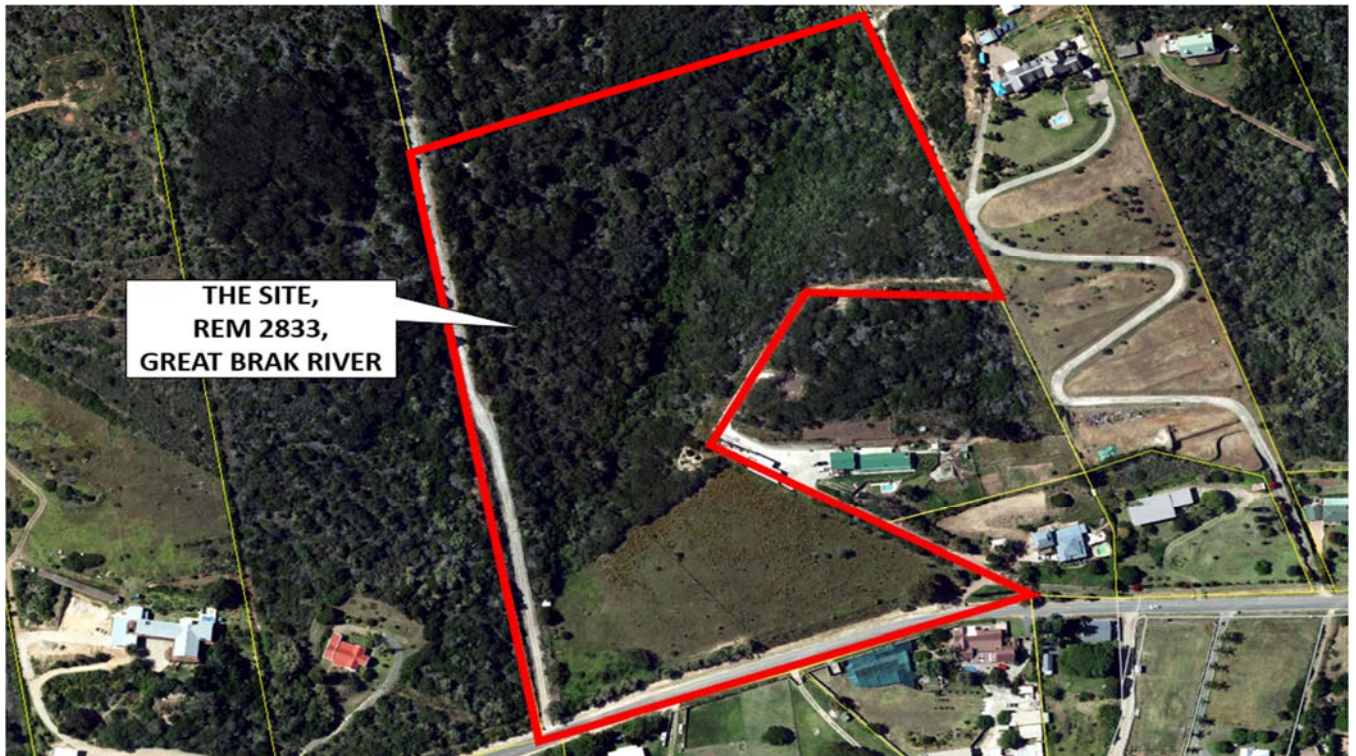


Figure 3-1 - Status Quo Photo



The site is currently zoned Agriculture Zone I as indicated in the extract of Mossel Bay Municipality’s GIS database.



Figure 3-2 - Current Zoning

Site is positioned within the Urban Edge with the latest SDF (2022) identifying the site for “Urban Expansion” (refer to Figure 3-3)

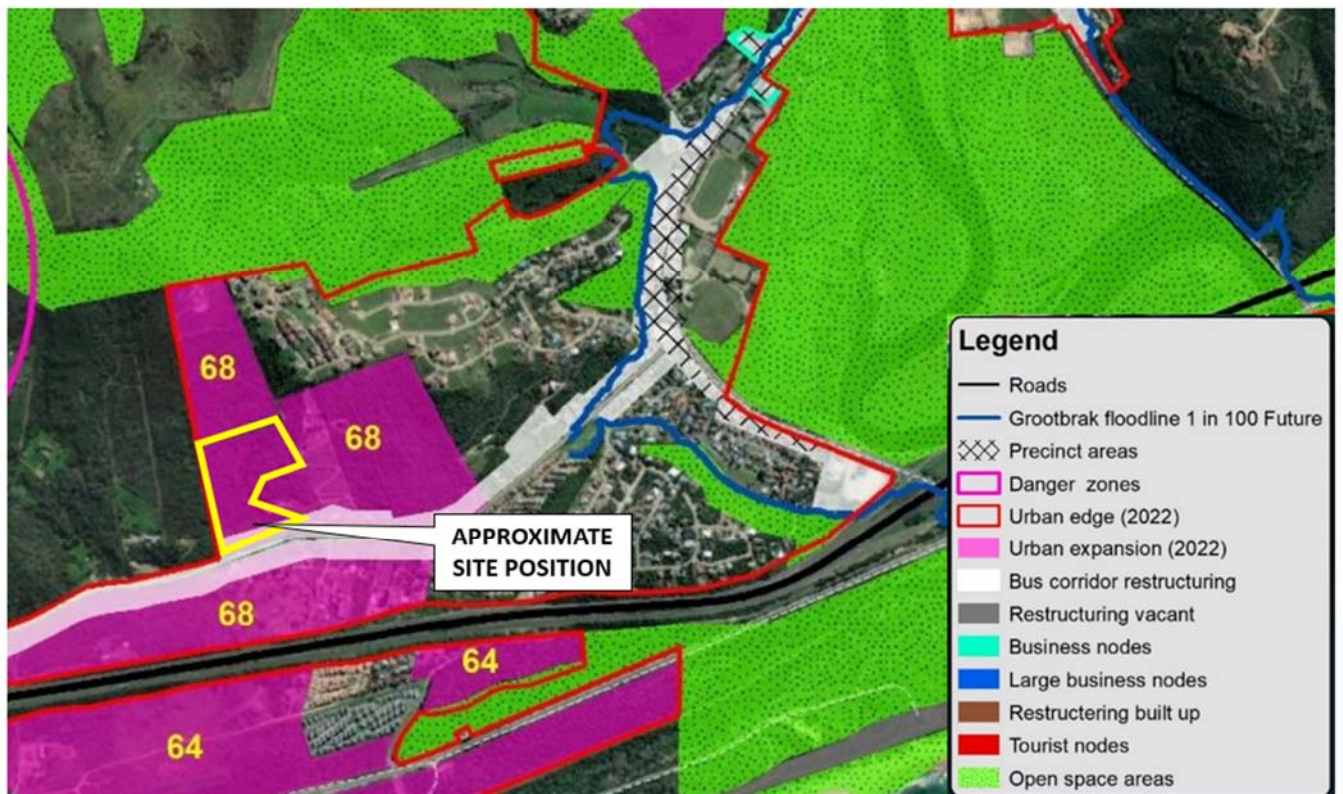


Figure 3-3 – Extract of Local Spatial Development Framework (2022)

#### 4 PROPOSED DEVELOPMENT PARTICULARS

It is the intention of the landowner to sub-divide the land portion into the following residential erven:

- 32 x General Residential Zone I erven
- 12 x Single Residential Zone I erven

A subdivision plan was prepared by Jan Vrolijk Town Planners and has been attached as **ANNEXURE B** to this report. For ease of reference, an extract of the SDP has been included as Figure 4-1 below.



Figure 4-1 - Proposed Site Development Plan

## 5 SURROUNDING ROAD NETWORK

Depending on which guidelines is being used, the nomenclature used in road classification varies slightly. The differences between the terms used in the 2006 Department of Transport (DoT) Guidelines and those specified in the South African Road Classification and Access Management Manual (COTO TRH 26, May 2018), are listed below:

| Road Class | Function | DoT 2006 Guidelines      | COTO 2012 (TRH 26 Manual) |
|------------|----------|--------------------------|---------------------------|
| Class 1    | Mobility | Primary Distributor      | Principal Arterial        |
| Class 2    |          | Regional Distributor     | Major Arterial            |
| Class 3    |          | District Distributor     | Minor Arterial            |
| Class 4    | Access   | District Collector       | Collector                 |
| Class 5    |          | Access Road              | Local Street              |
| Class 6    |          | Non-motorised access way | Walkway                   |

Table 5-1 - Road Classification Nomenclature

Roadways are classified by function on the basis of the priority given to land access versus through-traffic movement. Class 1 and 2 arterial roads provide a predominantly “mobility” function and Classes 4 and 5 roads perform a collector and local “access” function.

The functions of “mobility” and “access” overlap on minor arterials (Class 3 roads). This relationship between access and mobility has been indicated schematically in Figure 5-1.

Access Management is particularly important along Principal, Major and Minor Arterials and other primary roads that are expected to provide safe and efficient movement of traffic as well as limited access to property. However, Access Management is also necessary on lower-order roadways, such as Collector Streets and Local Streets, to address safety considerations, such as sight distance and corner clearance.

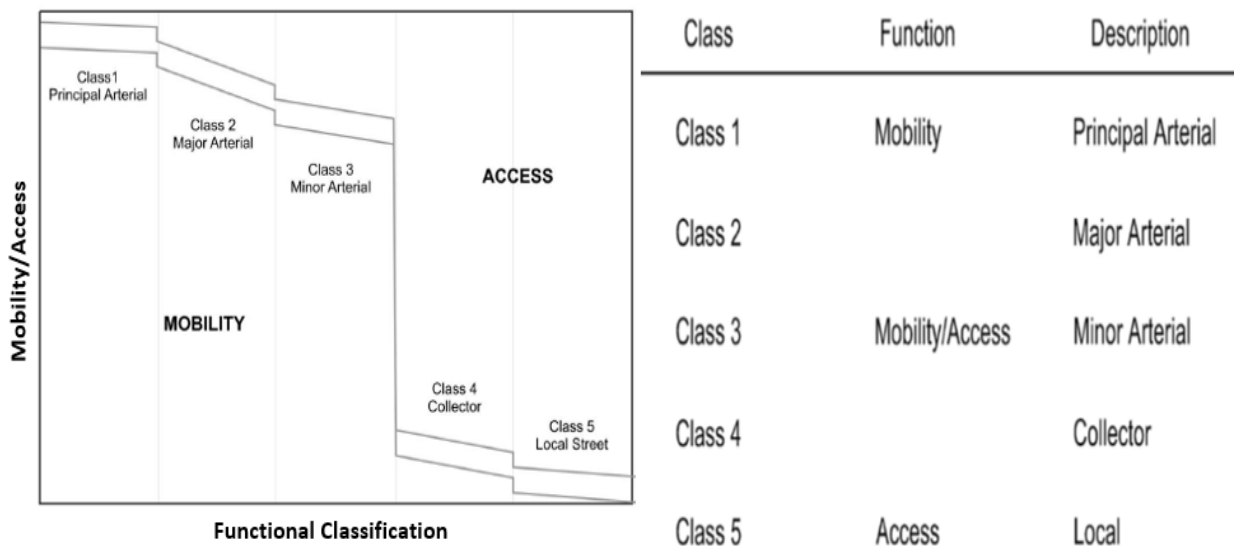


Figure 5-1 - Relationship Between Access and Mobility

### 5.1 DR1583 (SANDHOOGTE ROAD)

DR1583 is a provincial road that runs predominantly east/west. It acts as transportation link between DR1578 in the West and MR348 in the east.

The relevant section of DR1583 consists of a 7m wide asphalt surfaced road which was recently upgraded as part of the MR344/DR1578 upgrade. It has a posted speed limit of 60km/h.



Figure 5-2 - DR1578 Characteristics

According to the RNIS website, DR1583 has the following attributes:

- Road Reserve width = 20m
- Length = 6.95km
- Road Classification = Residential Access Collector
- Functional Classification = Level 4 (Tertiary) road
- RCAM classification = Rural Class 4 (a)



### Western Cape Provincial Administration Road Log Report

| SUMMARY PAGES                  |        |  |  |
|--------------------------------|--------|--|--|
| Road Number : DR01583 (DR1583) |        | Start Description: Jct. MR348 Groot Brak River |  |
|                                |        | End Description: Jct. DR1578 Klip Heuvel       |  |
| ROAD CATEGORY                  |        |  |  |
| Start Km                       | End Km | Category                                       |  |
| 1.60                           | 6.95   | RESIDENTIAL ACCESS COLLECTORS                  |  |
| FUNCTIONAL CLASS               |        |  |  |
| Start Km                       | End Km | Class  |  |
| 1.60                           | 6.95   | LEVEL4 (TERTIARY)                              |  |
| RCAM CLASSIFICATION            |        |  |  |
| Start Km                       | End Km | Class  |  |
| 1.60                           | 6.95   | R4a  |  |
| STATUTORY WIDTH                |        |  |  |
| Start Km                       | End Km | Width  |  |
| 1.60                           | 6.95   | 20.00  |  |
| ROAD NAME                      |        |  |  |
| Start Km                       | End Km | Road Name                                      |  |
| 1.60                           | 6.95   | SANDHOOGTE                                     |  |

Figure 5-3 - Extract of DR1583 Road Log (RNIS)

As indicated in Figure 5-3 above, the PGWC’s authority over DR1583 start at +-1.60km. This means that Mossel Bay Municipality is the road authority for the section of DR1583 situated between +-

0km and +-1,60km. The position of the relevant kilometer markers are indicated schematically in figure xx below



Figure 5-4 - Provincial vs Municipal Authority

The TRH 26 manual makes a clear distinction between rural and urban areas. Roads in rural and urban areas have the same six functional classes but at different scales and standards. Rural roads have longer reaches of connectivity and therefore require higher levels of mobility than urban roads. The TRH26 classification system therefore differentiates between rural and urban areas.

The TRH 26 continues to specify that when a rural road enters an urban area, it automatically becomes an urban road, preferably of the same class. If the urban area is on one side of the road only, it should be classified as urban if vehicle or pedestrian access is possible. If not, the rural road continues until the first access point. Hence a Throughway or Bypass remains rural in function if it does not provide convenient access to an urban area.

Where an urban road leaves the urban area, it automatically becomes a rural road, preferably with a class not lower than that of the urban area. Short sections of “rural” roads between urban areas can sensibly be treated as urban.

The urban/rural road classification changes at the boundary of the urban area but the road design should be adjusted some distance in advance of the urban area to provide a transition area and to give motorists time to slow down.

#### **The TRH 26 defines Class R4 (Rural) collector roads as follows:**

These roads form the link to local destinations. They do not carry through traffic but only traffic with an origin or destination along or near the road. A collector road must never be quicker to use to pass through an area than the alternative mobility road.

These roads would typically give access to smaller rural settlements, tourist areas, mines, game and nature parks and heritage sites. The roads can also provide direct access to large farms. Collector roads can also be provided within larger rural settlements to provide a collector function in such settlements.

The length of these roads would mostly be shorter than 10 km. Traffic volumes should not be more than about 1 000 vehicles per day.

### The TRH 26 defines Class U4 (Urban) collector roads as follows:

Collector streets are used to penetrate local neighbourhoods with the purpose of collecting (and distributing) traffic between local streets and the arterial system. The streets are mainly intended to serve an access function with limited mobility and traffic volumes; trip lengths and continuity must be limited.

They should ideally not carry any through traffic but only traffic with an origin or destination along or near to the street. The majority of the traffic using the collector street will have a destination in the street itself or in a local street leading off the collector. A collector street must not be quicker to use to pass through an area than a mobility road although it is recognized that in the absence of a mobility route, collectors must allow for some through traffic, albeit at low speeds.

Class 4a major collectors may also be used in preference to arterials when “mixed” through and local traffic is unavoidable, such as when arterials pass commercial centres with no alternative access. In this case, the local access traffic must be favoured at the expense of the mobility function.

From the TRH26 guidelines, it follows that the position of the urban edge is critical in road classification. Based on the 2022 Spatial Development Framework, (see Figure 5-5), the urban edge has recently moved out to include Erf 2833. The section of DR1583 next to Erf2833 is therefore situated with the urban area.

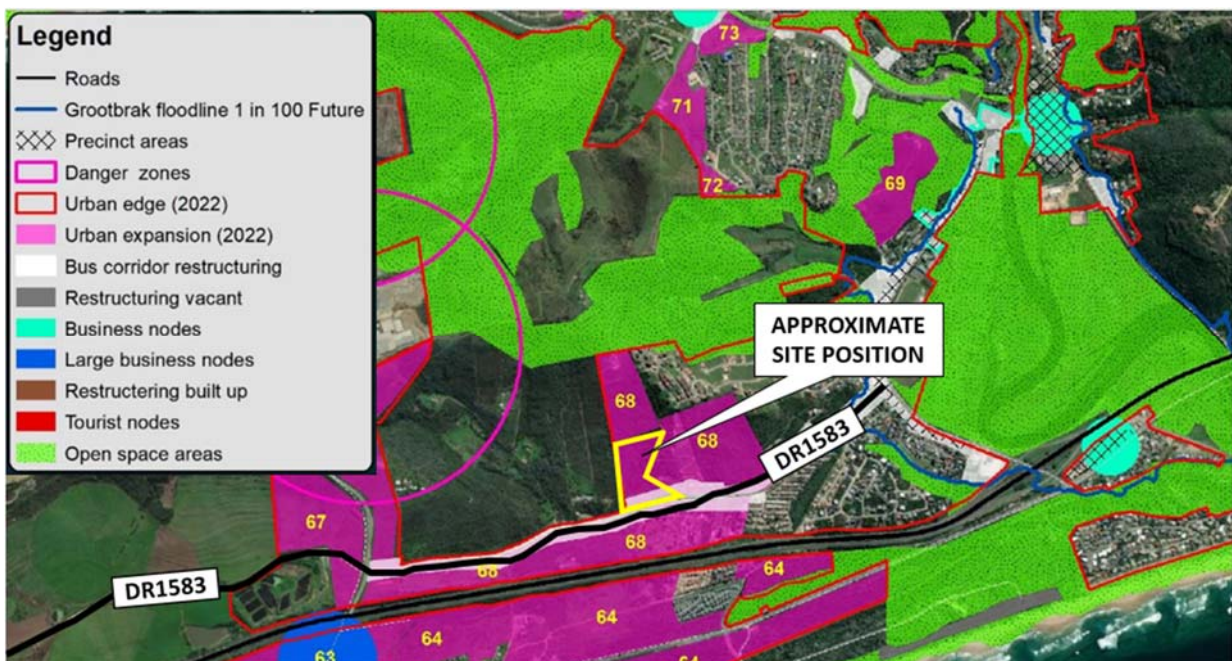


Figure 5-5 - Updated Urban Edge Position on 2022 SDF

## 5.2 EXISTING TRAFFIC VOLUMES

To determine the existing (background) traffic volumes in the vicinity of the site, classified traffic counts were recorded at three positions along DR1583 on Wednesday 05 May 2023. Counts were recorded over a 12-hour (06:00 to 18:00) period and vehicles were classified as either light or heavy. The counts took place at the following positions:

- Count 1 – Intersection of DR1578 and DR1583.
- Count 2 – On DR1583, in front of the site.
- Count 3 – Intersection of DR1583 and MR0348.

The traffic count intersections are indicated in Figure 5-6 below:



Figure 5-6 - Traffic Count Positions

The raw traffic count data has been attached as **ANNEXURE C** to this report. The data was analysed and the flow profiles extracted for the various approaches as indicated in the following graphs.

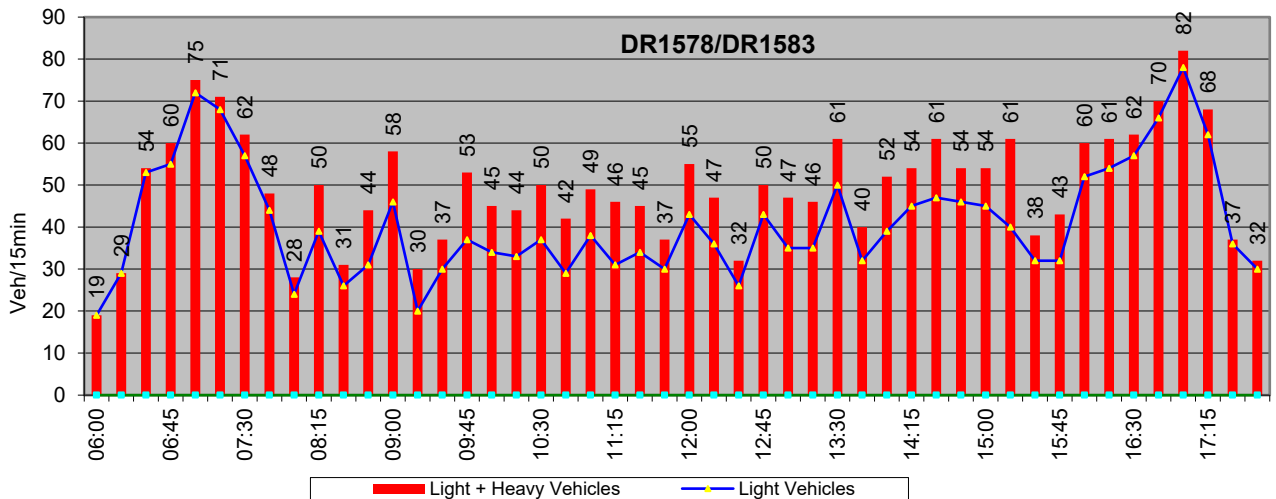


Figure 5-7 - Traffic Flow Analysis - DR1578/DR1583 Intersection

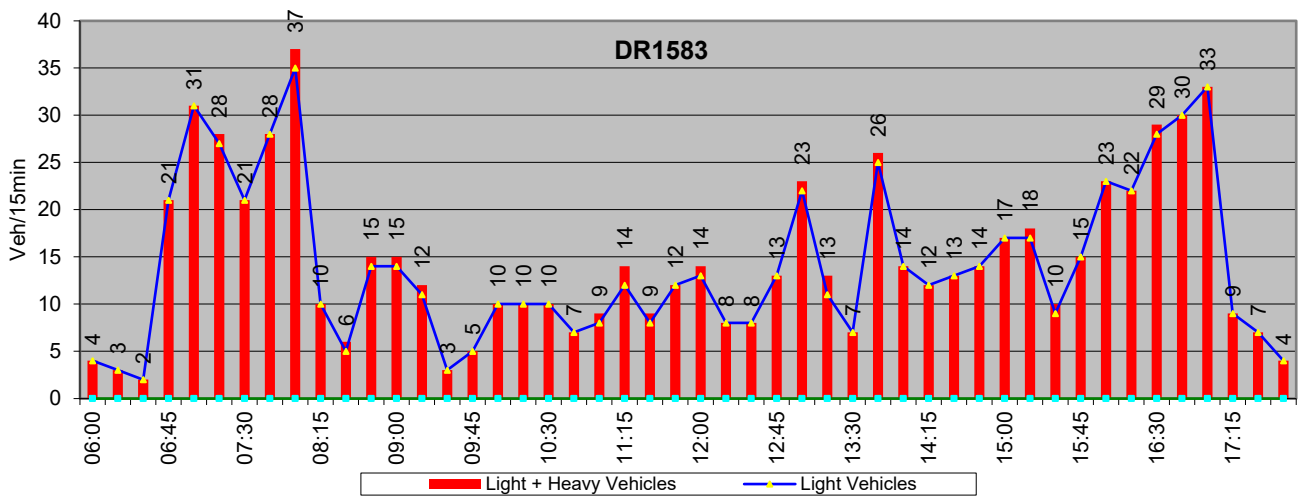


Figure 5-8 - Traffic Flow Analysis - DR1583 at Site Position

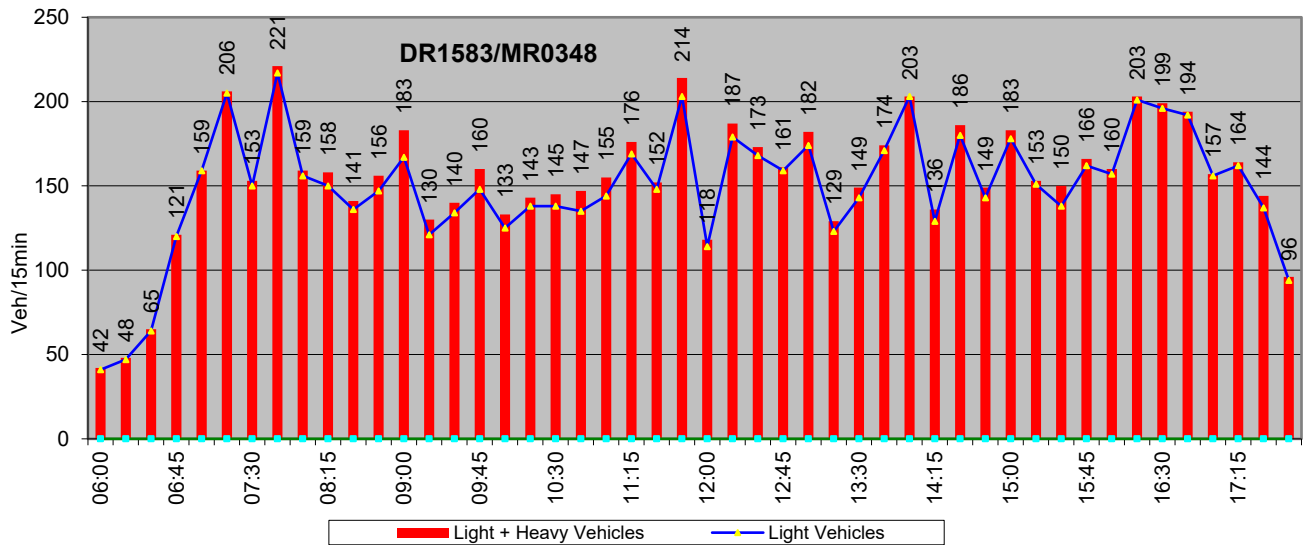


Figure 5-9 - Traffic Flow Analysis - DR1583/MR0348 Intersection

The traffic count revealed the following at the three intersections:

|                             | DR1578/DR1583 | DR1583 (at the Site) | DR1583/MR0349 |
|-----------------------------|---------------|----------------------|---------------|
| Total vehicles Counted      | 2374          | 704                  | 7423          |
| Light Vehicles (% of total) | 1977 (83%)    | 685 (97%)            | 7172 (97%)    |
| Heavy Vehicles (% of total) | 397 (17%)     | 19 (3%)              | 251 (3%)      |

Table 5-2 - Summary of Traffic Volumes

## 6 TRIP GENERATION POTENTIAL

Based on the SDP attached as ANNEXURE B, the development proposal consists of a mixture of Single Residential Zone I (SRZI) and General Residential Zone I (GRZI) erven.

### 6.1 TRIP GENERATION

The trip generation potential of the site has been calculated based on the guidelines published in TMH 17 (South African Trip Data Manual, COTO May 2018).

#### Single Residential Zone I

Based on the Mossel Bay Municipality Integrated Zoning Scheme By-Law, Single Zoneing is mainly used for **dwelling houses** and is defined as follows:

*The objective of this zone is to provide for residential development where the predominant type of accommodation is a dwelling house for a single family, where each dwelling has its own land unit, and adequate outdoor space. Limited employment and additional accommodation opportunities are possible as primary or consent uses, provided that the dominant use of the property remains residential, and impacts of employment and additional accommodation uses do not adversely affect the quality and character of the surrounding residential environment.*

The TMH land-uses that best fit the ethos of the proposed development is that of “single Dwelling House”. The relevant TMH 17 definition of the land use is listed below:

#### **210 Single Dwelling Unit** **Dwelling Units**

Single dwelling units are detached houses on individual erven. The units usually have individual access to streets.



The trip generation potential has been indicated in the table below.

| <b>210 Single Dwelling Unit</b> |         |         |           |          | <b>1D/Unit</b> |
|---------------------------------|---------|---------|-----------|----------|----------------|
| Description                     | AM Peak | PM Peak | Friday PM | Saturday | Sunday         |
| Trip Rate                       | 1.0     | 1.0     | 0         | 0.5      | 0.5            |
| IN/OUT                          | 25:75   | 70:30   | 0         | 50:50    | 50:50          |

**General Residential Zone I**

Based on the Mossel Bay Municipality Integrated Zoning Scheme By-Law, General Residential Zoning is mainly used for **town housing developments** and is defined as follows:

*“The objective of this zone is to encourage residential development of a greater density than for General Residential Zone II, while retaining the emphasis on design coordination and a modest scale in terms of height. This zone has particular location requirements, including proximity to transport and amenities, and should not be randomly located without due consideration of the availability of open space and community facilities. Town housing may be located in and around central business areas, near high density nodes and along activity axis including railway lines and main traffic routes, where flats are often found.”*

The TMH land-uses that best fit the ethos of the proposed development is that of “Townhouses”. The relevant TMH 17 definition of the land use is listed below:

**231 Townhouses (Simplexes and Duplexes) Dwelling Units**

Dwelling Units typically provided in clusters or in complexes. Units can be detached or provided within one building structure. Parking is often provided within a communal area.

The trip generation potential of townhouses are indicated in the table below.

| <b>231 Townhouses</b> |         |         |           |          | <b>1D/Unit</b> |
|-----------------------|---------|---------|-----------|----------|----------------|
| Description           | AM Peak | PM Peak | Friday PM | Saturday | Sunday         |
| Trip Rate             | 0.85    | 0.85    | 0         | 0.45     | 0.45           |
| IN/OUT                | 25:75   | 70:30   | 0         | 50:50    | 50:50          |

The trip generation potential of the total development can therefore be estimated as indicated in Table 6-1.

| Description      | Size     | Weekday AM |     | Weekday PM |     | Saturday |     |
|------------------|----------|------------|-----|------------|-----|----------|-----|
|                  |          | In         | Out | In         | Out | In       | Out |
| SRZI Erven       | 12 Units | 3          | 9   | 8          | 4   | 3        | 3   |
| GRZI Erven       | 32 Units | 7          | 20  | 8          | 19  | 7        | 7   |
| <b>Sub Total</b> |          | 10         | 29  | 16         | 23  | 10       | 10  |
| <b>Total</b>     |          | 39         |     | 39         |     | 20       |     |

Table 6-1 - Trip Generation Values

## 6.2 TRAFFIC DISTRIBUTION

Traffic distribution has been determined based on the actual traffic volumes counted at the various intersections. The AM and PM peak hour distributions and volume calculations have been indicated schematically in Figure A and Figure B in **ANNEXURE D**

## 7 INTERSECTION OPERATIONAL ANALYSES

The operational analysis was done with the “SIDRA INTERSECTION 9.1” (version 9.1.3) computer aided software that is developed specifically for traffic engineering capacity analysis. When elements of a road network such as intersections are analysed, their operating conditions are described in terms of Level of Service (LOS). The six letters from A to F are used to indicate different LOS. LOS A indicates very low traffic flows with correspondingly low delays. LOS E reflects capacity conditions, with high delays and unstable flow. LOS F reflects conditions where traffic demand exceeds capacity and traffic experiences congestion and delays. Generally, LOS A to D is considered acceptable in accordance with international standards. LOS E and F on the other hand are considered to be unacceptable.

The Average Delay is the delay (in seconds) that a motorist is likely to experience on an approach to the junction, while waiting for the junction to clear or other vehicles to maneuver. A further measure of the operating conditions at any point in a road network is the volume to capacity ratio (v/c). As the name implies it is the traffic demand volume divided by the available capacity of the road element. Generally, ratios of up to approximately 0.9 are internationally considered acceptable. Values exceeding 1.0 implies saturation of the facility.

It is important to note that trip reduction or SIDRA calibration factors were not applied to help improve the LOS of any of the analysed intersections. Vehicle Movement Data for heavy and light vehicles were left as per the default SDIRA default setting indicated in Figure 7-1 below.

| From South to Exit:          | W                        | N                        | E                        |
|------------------------------|--------------------------|--------------------------|--------------------------|
|                              | ↶<br>L2                  | ↑<br>T1                  | ↷<br>R2                  |
| Queue Space                  | 7,0 m                    | 7,0 m                    | 7,0 m                    |
| Vehicle Length               | 4,5 m                    | 4,5 m                    | 4,5 m                    |
| Vehicle Occupancy (pers/veh) | 1,2                      | 1,2                      | 1,2                      |
| Extra Midblock Delay         | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| Turning Vehicle Effect       | Factor ▾                 | Factor ▾                 | Factor ▾                 |
| Turning Vehicle Factor       | 1,05                     | 1,0                      | 1,05                     |
| Turn Radius                  |                          |                          |                          |
| Gap Acceptance Factor        | 1,0                      | 1,0                      | 1,0                      |
| Opposing Vehicle Factor      | 1,0                      | 1,0                      | 1,0                      |
| Prac. Deg. of Saturation     | Program ▾                | Program ▾                | Program ▾                |

**CALIBRATION FACTORS - LIGHT VEHICLES**

| From South to Exit:          | W                        | N                        | E                        |
|------------------------------|--------------------------|--------------------------|--------------------------|
|                              | ↶<br>L2                  | ↑<br>T1                  | ↷<br>R2                  |
| Queue Space                  | 13,0 m                   | 13,0 m                   | 13,0 m                   |
| Vehicle Length               | 10,0 m                   | 10,0 m                   | 10,0 m                   |
| Vehicle Occupancy (pers/veh) | 1,2                      | 1,2                      | 1,2                      |
| Extra Midblock Delay         | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| Turning Vehicle Effect       | Factor ▾                 | Factor ▾                 | Factor ▾                 |
| Turning Vehicle Factor       | 1,09                     | 1,0                      | 1,09                     |
| Turn Radius                  |                          |                          |                          |
| Gap Acceptance Factor        | 1,5                      | 1,5                      | 1,5                      |
| Opposing Vehicle Factor      | 1,5                      | 1,5                      | 1,5                      |
| Prac. Deg. of Saturation     | Program ▾                | Program ▾                | Program ▾                |

**CALIBRATION FACTORS - HEAVY VEHICLES**

Figure 7-1 - SIDRA Default Calibration Settings

The SIDRA analysis was performed for the following scenarios:

- **Status Quo:** The background traffic volumes were determined by means of manual traffic counting. These represent the actual volumes that are present on the road network.

- **No-Go Scenario:** A growth factor was applied to account for regional growth and the volumes were escalated up to the year 2028. This analysis indicates the traffic situation 5 years from now, but without the inclusion of the proposed development.
- **Operational Traffic** were estimated for the proposed development. The operational traffic volumes were added to the 2028 future traffic volumes to form the basis of the analysis, should the development be allowed to continue. Three (3) additional trips were included in the total operational traffic volumes.

The intersections were linked in SIDRA to create a network layout as indicated in Figure 7-2.

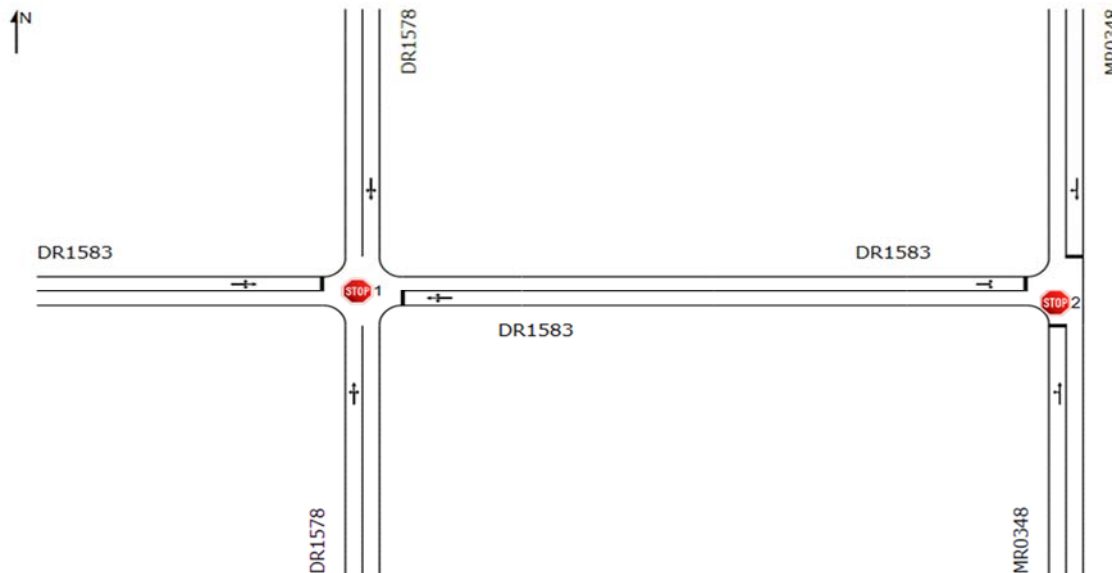


Figure 7-2 - Schematic Network Layout

### 7.1 STATUS QUO

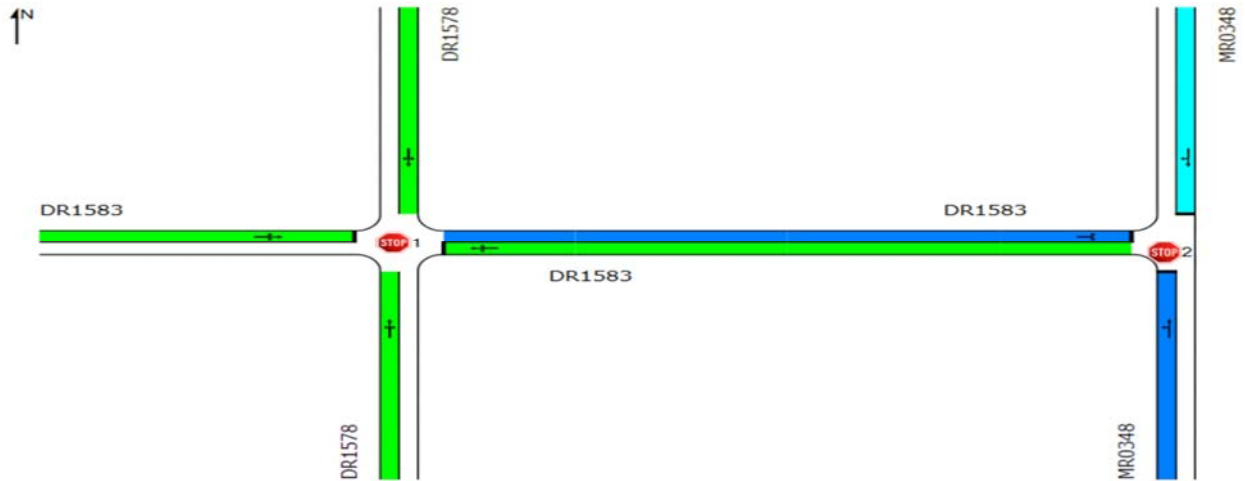
The current Weekday AM and PM Peak hour traffic volumes were used to calculate the Status Quo operational analysis. The results of the SIDRA Analysis have been attached as **ANNEXURE E** to this report, but has been summarised in the tables below:

| INTERSECTION  | APPROACH                      | MOVEMENT | 2023 WEEKDAY AM        |                     |             |                 | 2023 WEEKDAY PM        |                     |             |                 |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |
| DR1578/DR1583 | DR1578<br>(Southern Approach) | Left     | A                      | 6.1                 | 0.070       | 0.2             | A                      | 5.5                 | 0.081       | 0.2             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 6.2                 |             |                 | A                      | 6.4                 |             |                 |
|               | DR1583<br>(Eastern Approach)  | Left     | A                      | 8.3                 | 0.023       | 0.1             | A                      | 8.4                 | 0.029       | 0.1             |
|               |                               | Through  | A                      | 8.7                 |             |                 | A                      | 9.0                 |             |                 |
|               |                               | Right    | A                      | 8.8                 |             |                 | A                      | 9.0                 |             |                 |
|               | DR1578<br>(Northern Approach) | Left     | A                      | 5.5                 | 0.053       | 0.0             | A                      | 5.5                 | 0.063       | 0.0             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 5.7                 |             |                 | A                      | 6.0                 |             |                 |
|               | DR1583<br>(Western Approach)  | Left     | A                      | 8.3                 | 0.008       | 0.0             | A                      | 9.0                 | 0.089       | 0.3             |
|               |                               | Through  | A                      | 8.7                 |             |                 | A                      | 9.0                 |             |                 |
|               |                               | Right    | A                      | 8.8                 |             |                 | A                      | 9.2                 |             |                 |

Table 7-1 - DR1578/DR1583 LOS (Status Quo)

| INTERSECTION  | APPROACH                      | MOVEMENT | 2023 WEEKDAY AM        |                     |             |                 | 2023 WEEKDAY PM        |                     |             |                 |     |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|-----|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |     |
| DR1583/MR0348 | MR0348<br>(Southern Approach) | Left     | C                      | 18.1                | 0.46<br>8   | 2.1             | C                      | 16.2                | 0.4<br>71   | 2.1             |     |
|               |                               | Through  | C                      | 17.7                |             |                 | C                      | 15.9                |             |                 |     |
|               | MR0348<br>(Northern Approach) | Through  | B                      | 14.2                | 0.39<br>9   | 1.6             | B                      | 12.4                | 0.34<br>5   | 1.3             |     |
|               |                               | Right    | B                      | 13.9                |             |                 | B                      | 12.5                |             |                 |     |
|               | DR1583<br>(Western Approach)  | DR1583   | Left                   | C                   | 19.9        | 0.44<br>9       | 2.0                    | C                   | 19.8        | 0.38<br>7       | 1.6 |
|               |                               |          | Right                  | C                   | 19.2        |                 |                        | C                   | 19.2        |                 |     |

Table 7-2 - DR1583/MR0348 LOS (Status Quo)



### 7.2 NO GO SCENARIO (ESCALATED 2028 TRAFFIC VOLUMES)

In order to estimate the future (2028) traffic volumes for the No-Go Scenario, the 2023 Status Quo Peak Hour traffic volumes were further increased with an annual growth factor. Reference is made to the South African Department of Transport’s Manual for Traffic Impact Studies (DoT, October 1995) which provides a table with typical growth rates. This document recognises that the method for determining traffic growth is important, but also states that there are a number of factors which influence the traffic growth rate. The approach is therefore to classify the study area with a low, average, high or extremely high growth rate. The typical growth rates are indicated in Table 7-3.

| Category           | Yearly Growth Rate (%) |
|--------------------|------------------------|
| Low                | 0-2.5                  |
| Average            | 2.5-3.5                |
| High               | 3.5-6                  |
| Exceptionally high | >6                     |

Table 7-3 - Typical Traffic Growth Rates

Based on the growth within the Western Cape region, it was decided to apply a fairly conservative 3% annual growth rate to the Status Quo traffic volumes.

The estimated 2028 traffic volumes (for the No-Go Scenario) were calculated according to the equation below:

$$F = P \times (1 + i)^n$$

Where: F = Future Trips  
 P = Present Trips  
 n = 5 years  
 i = 3% Growth

The escalated (2028) background traffic volumes have been attached as **Figure C** in **ANNEXURE D**. This scenario was tested and analyzed in SIDRA to determine the Level of Service (both AM and PM peak hour periods) of the various intersections, should the proposed development not take place. The results of the analyses have been attached as **ANNEXURE E**, but a summary of the findings has been included in Table 7-4 and Table 7-5.

| INTERSECTION  | APPROACH                      | MOVEMENT | 2028 WEEKDAY AM        |                     |             |                 | 2028 WEEKDAY PM        |                     |             |                 |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |
| DR1578/DR1583 | DR1578<br>(Southern Approach) | Left     | A                      | 6.1                 | 0.091       | 0.2             | A                      | 5.5                 | 0.095       | 0.2             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 6.4                 |             |                 | A                      | 6.5                 |             |                 |
|               | DR1583<br>(Eastern Approach)  | Left     | A                      | 8.4                 | 0.030       | 0.1             | A                      | 8.5                 | 0.036       | 0.1             |
|               |                               | Through  | A                      | 9.1                 |             |                 | A                      | 9.2                 |             |                 |
|               |                               | Right    | A                      | 9.3                 |             |                 | A                      | 9.3                 |             |                 |
|               | DR1578<br>(Northern Approach) | Left     | A                      | 5.5                 | 0.067       | 0.0             | A                      | 5.5                 | 0.079       | 0.0             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 5.8                 |             |                 | A                      | 6.3                 |             |                 |
|               | DR1583<br>(Western Approach)  | Left     | A                      | 8.4                 | 0.010       | 0.0             | A                      | 9.1                 | 0.109       | 0.4             |
|               |                               | Through  | A                      | 9.1                 |             |                 | A                      | 9.3                 |             |                 |
|               |                               | Right    | A                      | 8.9                 |             |                 | A                      | 9.6                 |             |                 |

Table 7-4 - DR1578/DR1583 LOS (2028 NO-GO)

| INTERSECTION  | APPROACH                      | MOVEMENT | 2028 WEEKDAY AM        |                     |             |                 | 2028 WEEKDAY PM        |                     |             |                 |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |
| DR1583/MR0348 | MR0348<br>(Southern Approach) | Left     | C                      | 20.0                | 0.542       | 2.8             | C                      | 17.7                | 0.543       | 2.7             |
|               |                               | Through  | C                      | 19.6                |             |                 | C                      | 17.5                |             |                 |
|               | MR0348<br>(Northern Approach) | Through  | C                      | 15.2                | 0.461       | 2.0             | B                      | 13.1                | 0.399       | 1.6             |
|               |                               | Right    | B                      | 14.8                |             |                 | B                      | 13.1                |             |                 |
|               | DR1583<br>(Western Approach)  | Left     | C                      | 21.9                | 0.520       | 2.6             | C                      | 21.1                | 0.447       | 2.0             |
|               |                               | Right    | C                      | 21.1                |             |                 | C                      | 20.6                |             |                 |

Table 7-5 - DR1583/MR0348 LOS (2028 NO-GO)

The above results have been represented schematically in the network LOS Lane Display for the (AM peak hour period) in Figure 7-3.

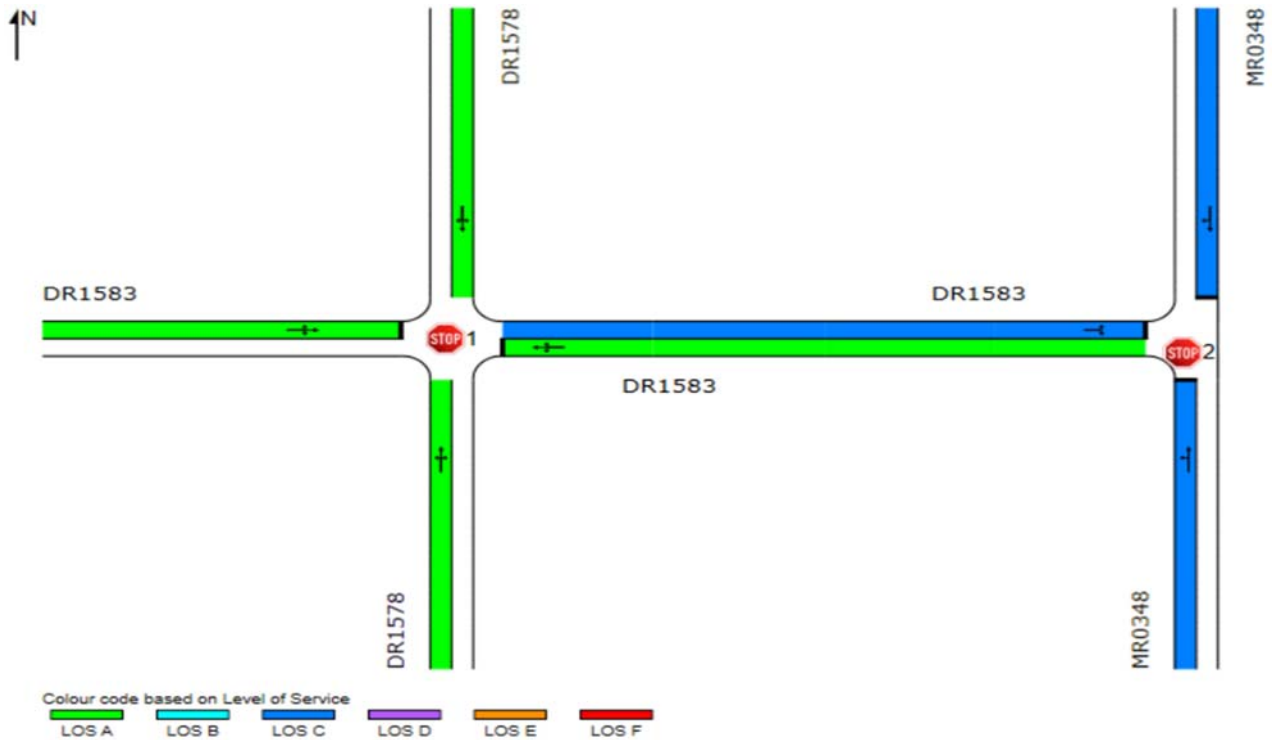


Figure 7-3 - Lane LOS Display for 2028 AM Scenario

### 7.3 OPERATIONAL PHASE TRAFFIC

In order to determine the impact of the proposed development on the surrounding road network, the trip generation potential of the proposed development was added to the future 2028 background traffic volumes. The final traffic volumes can be seen in **Figure E** in **ANNEXURE D**. The results of the SIDRA analysis have been summarized below.

| INTERSECTION  | APPROACH                      | MOVEMENT | 2028 + DEV WEEKDAY AM  |                     |             |                 | 2028 + DEV WEEKDAY PM  |                     |             |                 |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |
| DR1578/DR1583 | DR1578<br>(Southern Approach) | Left     | A                      | 6.1                 | 0.092       | 0.2             | A                      | 5.5                 | 0.098       | 0.3             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 6.4                 |             |                 | A                      | 6.5                 |             |                 |
|               | DR1583<br>(Eastern Approach)  | Left     | A                      | 8.4                 | 0.035       | 0.1             | A                      | 8.5                 | 0.038       | 0.1             |
|               |                               | Through  | A                      | 9.1                 |             |                 | A                      | 9.3                 |             |                 |
|               |                               | Right    | A                      | 9.3                 |             |                 | A                      | 9.3                 |             |                 |
|               | DR1578<br>(Northern Approach) | Left     | A                      | 5.5                 | 0.068       | 0.0             | A                      | 5.5                 | 0.074       | 0.0             |
|               |                               | Through  | A                      | 0.0                 |             |                 | A                      | 0.0                 |             |                 |
|               |                               | Right    | A                      | 5.8                 |             |                 | A                      | 6.3                 |             |                 |
|               | DR1583<br>(Western Approach)  | Left     | A                      | 8.4                 | 0.010       | 0.0             | A                      | 9.1                 | 0.110       | 0.4             |
|               |                               | Through  | A                      | 9.1                 |             |                 | A                      | 9.4                 |             |                 |
|               |                               | Right    | A                      | 9.3                 |             |                 | A                      | 9.7                 |             |                 |

Table 7-6 - DR1578/DR1583 LOS (Development + Escalated 2028 Volumes)

| INTERSECTION  | APPROACH                      | MOVEMENT | 2023 WEEKDAY AM        |                     |             |                 | 2023 WEEKDAY PM        |                     |             |                 |
|---------------|-------------------------------|----------|------------------------|---------------------|-------------|-----------------|------------------------|---------------------|-------------|-----------------|
|               |                               |          | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) | LEVEL OF SERVICE (LOS) | AVE DELAY (seconds) | V / C RATIO | AVE QUEUE (veh) |
| DR1583/MR0348 | MR0348<br>(Southern Approach) | Left     | C                      | 21.3                | 0.568       | 3.0             | C                      | 18.6                | 0.568       | 3.0             |
|               |                               | Through  | C                      | 20.9                |             |                 | C                      | 18.3                |             |                 |
|               | MR0348<br>(Northern Approach) | Through  | C                      | 15.6                | 0.476       | 2.2             | B                      | 13.2                | 0.412       | 1.7             |
|               |                               | Right    | C                      | 15.3                |             |                 | B                      | 13.2                |             |                 |
|               | DR1583<br>(Western Approach)  | Left     | C                      | 22.4                | 0.551       | 2.9             | C                      | 21.6                | 0.465       | 2.2             |
|               |                               | Right    | C                      | 21.6                |             |                 | C                      | 21.0                |             |                 |

Table 7-7 - DR1583/MR03483 LOS (Development + Escalated 2028 Volumes)

### 7.4 SUMMARY OF ANALYSIS

#### Status Quo

Intersection analysis based on the status quo traffic count revealed that both intersections operate at acceptable Level of Service during both the AM and PM Peak Hour Periods. The worst LOS is experienced at the MR348/DR1583 intersection where delays of 19.9s are experienced on the DR1578 approach to the intersection.

#### No Go

The No-Go Scenario was simulated by increasing the Status Quo volumes with a fairly conservative 3% growth rate over a 5-year period. Analysis of the scenario indicates LOS of both intersections remain at an acceptable LOS, but once again the worst LOS is experienced at the MR348/DR1583 intersection where delays increased from 19.9s to 21.9s on the DR1578 approach to the intersection.

#### Operational Phase

The operational phase analysis made provision for the increase in traffic volumes generated by the proposed development. Since the proposed development is seen as a fairly low trip generator (42 trips during the peak hour period), the addition of the new generated traffic to the future background volumes, does not have a major impact on the LOS of the affected intersection. The worst LOS remains on the DR1578 approach to the MR0348 intersection, where delays are expected to increase from 21.9s to 22.4s. is expected for the right turn movement of the DR1578 Northern approach to the intersection.

Comparing the 2028 No-Go to the 2028 Operational (2028 background + development traffic), it is easy to see from Figure 7-4 that the additional traffic expected to the generated by the development is not expected to have a noticeable impact on the Level of Service of either of the two intersections.

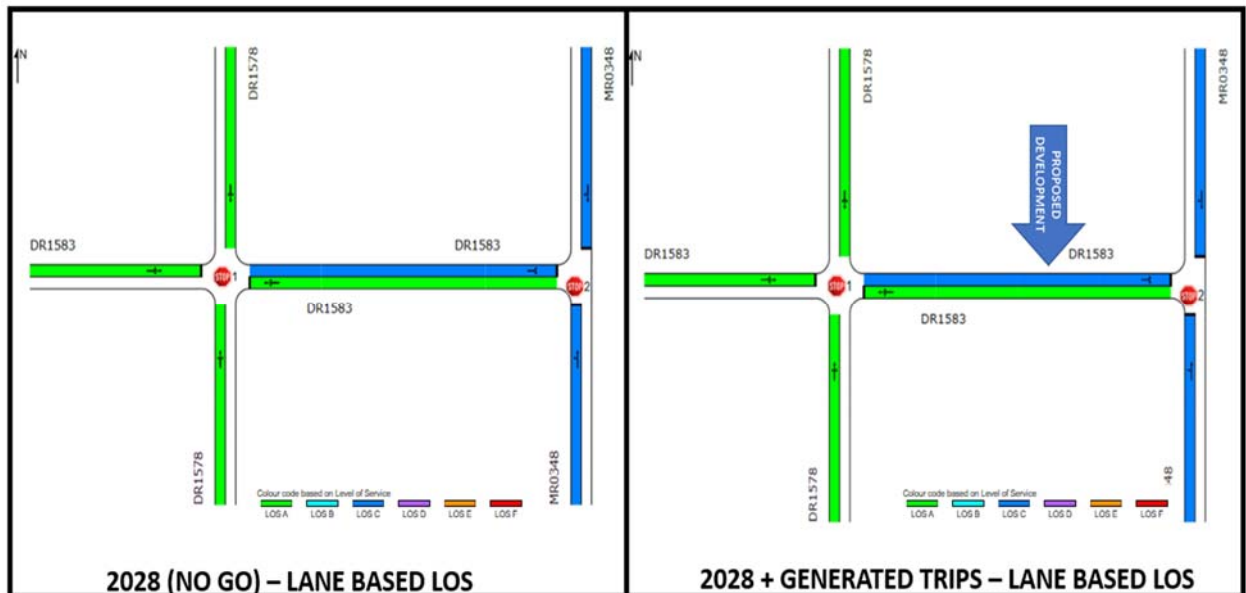


Figure 7-4 - Comparison between NO-GO and Operational LOS

## 8 GEOMETRIC CONSTRAINTS

### 8.1 DRIVEWAY CLASSIFICATION

According to the PGWC’s Road Access Guidelines (2020), “the term “driveway” describes the intersecting roadway giving direct access to a privately-owned property adjacent to the road where such intersecting roadway is not a public road or street.

A driveway is usually the only access point to the property, although it is possible that connections could be made between adjacent properties through connecting roads provided by agreement between property owners or via a servitude registered for a road access. Larger developments may take access through more than one driveway from more than one road.

*“Conventional driveways” are defined in these Guidelines as domestic equivalent driveways, low-volume driveways and high-volume driveways, with high-volume driveways being regarded as having an equivalent status to a Class 5 road”.*

*“Equivalent driveways” of a higher order than high-volume driveways may be equivalent to Classes 2, 3 or 4 public road intersections”*

The 2020 AMG lists the three categories of “conventional driveways”, defined by the number of vehicular trips generated per hour that use or are projected to use a driveway, as follows:

*“Domestic equivalent driveways are driveways giving vehicular access to private homes, micro businesses and farms which attract very small traffic volumes. In residential areas with small plot sizes the vehicle using the driveway may have to back into the through road when leaving the property.*

*Domestic equivalent driveways have a small impact on the through road but can result in conflicts where reversing manoeuvres take place into the through road. For this reason, domestic equivalent driveways are acceptable on Class 5 roads, but should be discouraged on Class 4 roads except where special provision is made for access to properties within the road reserve. This requires that there is sufficient space clear of the through traffic lanes for*



a vehicle reversing out of a property to manoeuvre within the road reserve so as to enter the traffic stream safely.

In rural areas, low-volume farm driveways generating less than five vehicles per day are regarded as domestic equivalent driveways.

**Low-volume driveways** may carry larger traffic volumes than domestic equivalent driveways and are expected to serve larger developments. The lower volume driveway categories (domestic equivalent driveways and low-volume driveways) have no class equivalent as they generally carry lower volumes than the traffic volume carried by any class of public road.”

In rural areas, farm accesses combined with small-scale developments such as farm stalls or stand-alone retail outlets may be low-volume driveways depending on the traffic volumes generated.

**High-volume driveways** are equivalent to Class 5 local roads and are expected to carry larger traffic volumes than low-volume driveways.

Based on the expected trip generation (refer to Section 6.1), the proposed site access classifies as a **High Volumes** driveway, as indicated in Figure 8-1.

| Driveway category    | Class equivalent | Roadside development environment |              |          |            |        |
|----------------------|------------------|----------------------------------|--------------|----------|------------|--------|
|                      |                  | CBD                              | Intermediate | Suburban | Semi-rural | Rural  |
|                      |                  | Vehicles per hour                |              |          |            |        |
| Domestic equivalent  |                  | < 5                              | < 5          | < 5      | < 5        | < 5    |
| Low-volume           |                  | 5–30                             | 5–30         | 5–30     | 5–30       | 5–30   |
| High-volume          | 5                | 30–150                           | 30–100       | 30–60    | 30–50      | 30–50  |
| Equivalent collector | 4                | 150–750                          | 100–625      | 60–500   | 50–250     | 50–500 |

Figure 8-1 - Driveway Classification

The WCG Access Management Guidelines (2020) provides guidelines on where driveways should be allowed for a given combination of road class and roadside development environment. The table shows that both high and low volume driveways are permitted on Class 4 roads.

| Roadside development environment | Class 2 Major | Class 3 Minor |        | Class 4 Collector |        |        | Class 5 Local |        |        |        |
|----------------------------------|---------------|---------------|--------|-------------------|--------|--------|---------------|--------|--------|--------|
|                                  | LVD+HVD       | DED           | LVD    | HVD               | DED    | LVD    | HVD           | DED    | LVD    | HVD    |
| CBD                              | Red           | Red           | Red    | Green             | Green  | Green  | Green         | Green  | Green  | Green  |
| Intermediate                     | Red           | Red           | Red    | Green             | Green  | Green  | Green         | Green  | Green  | Green  |
| Suburban                         | Red           | Red           | Red    | Green             | Green  | Green  | Green         | Green  | Green  | Green  |
| Semi-rural                       | Red           | Yellow        | Yellow | Green             | Green  | Green  | Green         | Green  | Green  | Green  |
| Rural                            | Yellow        | Yellow        | Yellow | Yellow            | Yellow | Yellow | Yellow        | Yellow | Yellow | Yellow |

Figure 8-2 - AMG Guidelines for Allowing Driveways

### 8.2 MOSSEL BAY MUNICIPALITY SPECIFICATIONS REGARDING VEHICLE ENTRANCES

The Mossel Bay Municipality Integrated Zoning Scheme By-Law specifies the following with regards to vehicle entrance and exit ways to and from a property:

- a) motor vehicle carriageway crossings must be limited to one per site per public street or road abutting the site;
- b) despite paragraph (a), where the total length of any street boundary of a site exceeds 30 metres in length, one additional carriageway crossing may be permitted,
- c) provided that no two carriageway crossings are closer than 12 metres to each other;
- d) the minimum and maximum widths of motor vehicle carriageway crossings must be in accordance with the table, titled “Width of motor vehicle carriageway crossings”; and
- e) the minimum width of a panhandle access may not be less than 3 metres wide.

| Width of vehicle Carriageway Crossings |               |               |
|--|---------------|---------------|
| Type of Carriageway Crossing           | Minimum Width | Maximum Width |
| Single entrance or exit way            | 2,7meters     | 4,0 meters    |
| Combined entrance and exit way         | 5,0meters     | 8,0 meters    |

### 8.3 DRIVEWAY GRADE AND SPEED DIFFERENTIAL

Along older urban arterial streets, it is common to find steep driveways with grades (or slopes) of 5–10% or more. Driveways with steep grades were often constructed to allow the driveway and connecting parking lots to drain more efficiently and to save earth-moving costs. On the other hand, more recently constructed arterials typically feature very gentle driveway grades. Driveway grade is an important, yet often overlooked, safety consideration.

The maximum practical grade for driveways varies between 8–14 % for low-volume driveways and five percent for high-volume driveways. Furthermore, the maximum practical change in grade is about 10%. Above this value, many vehicles will scrape their bumpers or other low-hanging parts on the driveway, potentially causing damage to the vehicle and driveway or roadway surface. The PGWC’s book of standard geometric road plans specifies the following with regards to the slope of two intersecting roads:

4. WHERE TWO ROADS INTERSECT THE NUMERICAL DIFFERENCE OF THE GRADIENTS (ROLL OVER) SHOULD NOT EXCEED 10% WITH A MAXIMUM SUPERELEVATION OF 6% ON THE MAIN ROAD.

5. MAXIMUM APPROACH GRADIENT TO BE 4% UPGRADE AND 6% DOWNGRADE.

Figure 8-3 - PGWC Standard Plan book

#### Why is driveway grade important?

Driveway grade is important because it affects *speed differential*. Turning vehicles must slow appreciably to enter a driveway. The steeper the driveway, the greater the reduction in speed required to prevent “bottoming out.” The following table shows typical driveway entry speeds for varying degrees of driveway grade.

| Driveway Grade Change | Typical Driveway Entry Speed |
|-----------------------|------------------------------|
| Greater than 15%      | Less than 13km/h             |
| 14-15%                | 13km/h                       |
| 12-13%                | 15km/h                       |
| 10-11%                | 16km/h                       |
| 8-9%                  | 18km/h                       |
| 6-7%                  | 19km/h                       |

Table 8-1 - Driveway entry Speeds (Oregon State University)

Speed differential is the difference between the speed of vehicles that are continuing along the main roadway versus that of those that are turning into or out of the driveway. For instance, if through traffic generally moves at 60 km per hour and cars have to slow to 20 km per hour to

enter a driveway, the speed differential at that driveway is 40 km per hour. A speed differential above 30 km per hour begins to present safety concerns. When the speed differential becomes greater than 50 to 60 km per hour, the likelihood of crashes involving fast moving through vehicles and turning vehicles increases very quickly. Rear-end collisions are very common on roads and streets with large driveway speed differentials and a high density of commercial driveways. When the speed differential is high, it is also more likely that crashes will be more severe, cause greater property damage, and have a greater chance of injury or fatalities. Keeping the speed differential low is very important for safety reasons.

### 8.4 EXISTING 20M WIDE ROAD SERVITUDE

An existing 20m wide road servitude provides access to Erf4650, Erf 2833 and Remainder of 2832 as indicated in Figure 8-4.

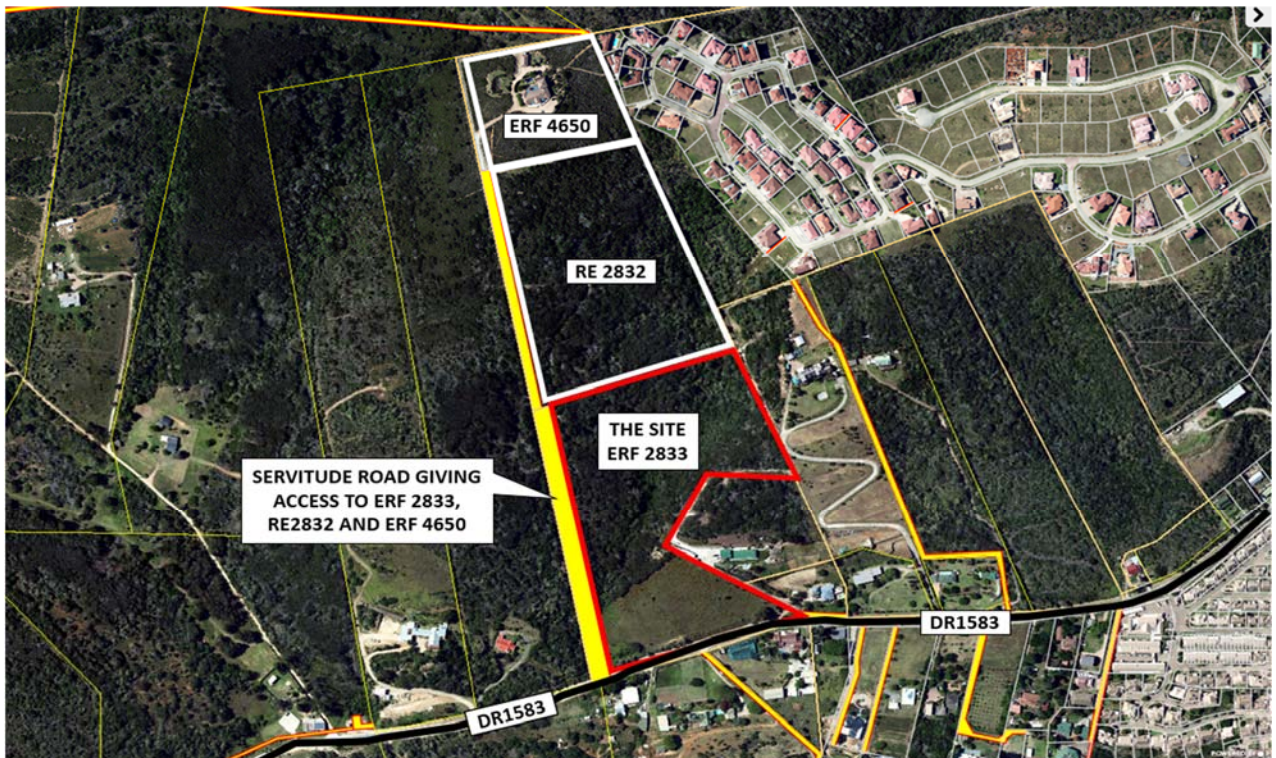


Figure 8-4 - 20m Wide Road Servitude

A 3m wide, interlocking block paving road is currently situated within the 20m wide road reserve. This road is used on a daily basis by the resident staying on Erf 4650 at the end of the road.



Figure 8-5 - Existing Servitude Road

Based on the proposed SDP, the existing servitude road will be used to provide access to all erven.

### 8.4.1 SIGHT LINES FOR EXISTING SERVITUDE ROAD.

Based on the 60km/h posted speed limit (refer to Section 5.1 of this report), a Shoulder Sight Distance of 125m is required for passenger vehicles entering a 7.5m wide road.

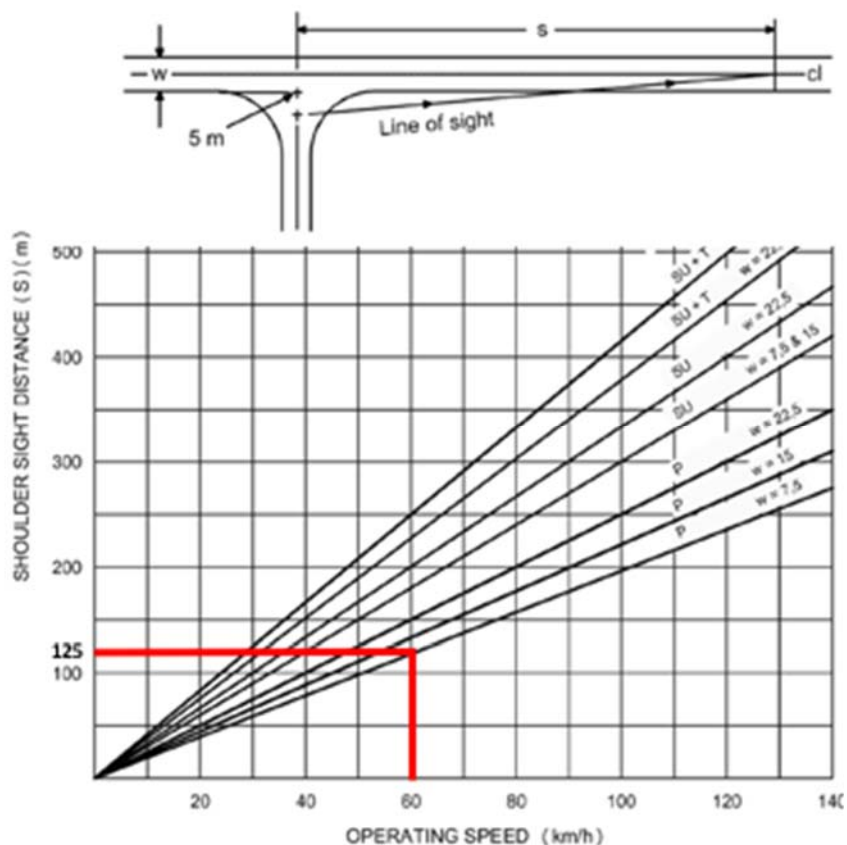


Figure 8-6 - Shoulder Sight Distance for Stop Condition

From Figure 8-7 and Figure 8-8, it follows that SSD in excess of 125m was measured in both directions from the existing servitude road. (Note the minor timber structure currently obscuring sight lines towards the DR1578)



Figure 8-7 - SSD towards DR1578



Figure 8-8 - SSD towards MR0348

### 9 THROAT LENGTHS

The proposed SDP does not make provision for access control and hence throat length calculations are not applicable. The position of the secondary road parallel to Sandhoogte Road, is however situated approximately 40m away from Sandhoogte road edge, ensuring that the two intersections are not situated within each other’s envelope.

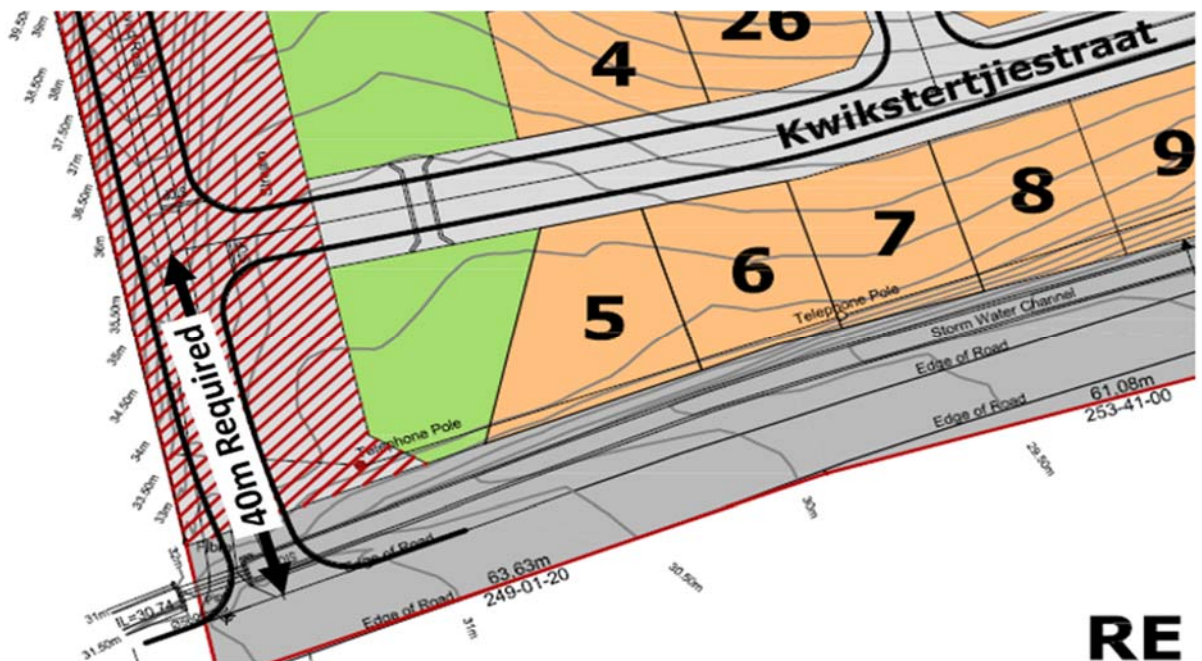


Figure 9-1 - Throat Length Requirement

RE

## 10 SUMMARY

The various components of this Transportation Investigation can be summarised as follows:

1. It is the client's intention to subdivide erf 2833, Great Brak River in order to create a new residential development consisting of the following land uses:
  - 32 x General Residential Zone I erven
  - 12 x Single Residential Zone I erven
2. The latest SDF (2022) made provision for the moving of the Urban Edge to include the proposed site.
3. The site is situated next to DR1583/Sandhoogte Road. However, the portion of DR1583/Sandhoogte between +0km and +-1.6km falls under the authority of Mossel Bay Municipality, and PGWC authority only starts at +-1.6km onwards. DR1583 is classified as a Class4 Rural Collector on the PGWC's RNIS Website.
4. SDP makes provision for site accesses via an existing servitude road along the western property boundary.
5. The combined estimated trip generation potential of the site has been calculated as follows:
  - a. Weekday AM = 39 Trips (IN and OUT)
  - b. Weekday PM = 39 Trips (IN and OUT)
6. 12 Hour traffic counts recorded at three positions along DR1583 on Wednesday 05 May 2023. The total volumes counted at the three intersections are summarised below:

|                             | <b>DR1578/DR1583</b> | <b>DR1583 (at the Site)</b> | <b>DR1583/MR0349</b> |
|-----------------------------|----------------------|-----------------------------|----------------------|
| Total Vehicles Counted      | 2374                 | 704                         | 7423                 |
| Light Vehicles (% of total) | 1977 (83%)           | 685 (97%)                   | 7172 (97%)           |
| Heavy Vehicles (% of total) | 397 (17%)            | 19 (3%)                     | 251 (3%)             |

7. Based on operating speed, road width and type of vehicle, a minimum Shoulder Sight Distance of 125m is required. SSD in excess of 125m were measured in both directions at the existing servitude road intersection.
8. Both the DR1578/DR1583 and DR1583/MR0348 intersections were analysed in SDIRA. Analysis revealed acceptable LOS for both the Status Quo and Future (2028) "NO-GO" Scenarios.
9. SIDRA analysis of the future operational (2028 Background + Generated Traffic) scenario, indicated that the inclusion of the additional trips, are not expected to have a noticeable impact on the overall LOS of the affected intersections.
10. The proposed site access is classified as a high-volume driveway.
11. The proposed SDP does not make provision for any type of access control.

## 11 RECOMMENDATIONS

Based on the findings of this report, the proposed rezoning and subdivision of Erf 2833, Great Brak River is supported from a traffic and transportation point of view, subject to the following conditions:

- 1.1. The minor timber structure obscuring SSD at the current Servitude Road/DR1583 junction (refer to Paragraph 8.4.1), should be moved to a new position where it does not affect SSD.
- 1.2. Road Widths :
  - 1.2.1. Tarentaal Street (the existing servitude road) should be widened from 3m to 6.4m, in order to accommodate two clearly defined 3,4m wide lanes.
  - 1.2.2. Due to the small number of vehicles expected to make use of them, the road width of Kwikstertjie Street, Geelvink Street, Mossie Slot and Laksman Street can be reduced to a absolute minimum of 5.5m (2x2.75m wide lanes).
- 1.3. Vegetation and shrubbery within the road reserve that could have a negative future impact on the SSD (towards DR1578) should be kept in a neat and trimmed condition by the developer.
- 1.4. To protect mobility at the DR1583/Servitude Road intersection, it is proposed that the ingress movement along Tarentaal Street receives priority, by implementing the road marking configuration indicated schematically in Figure 11-1 below.

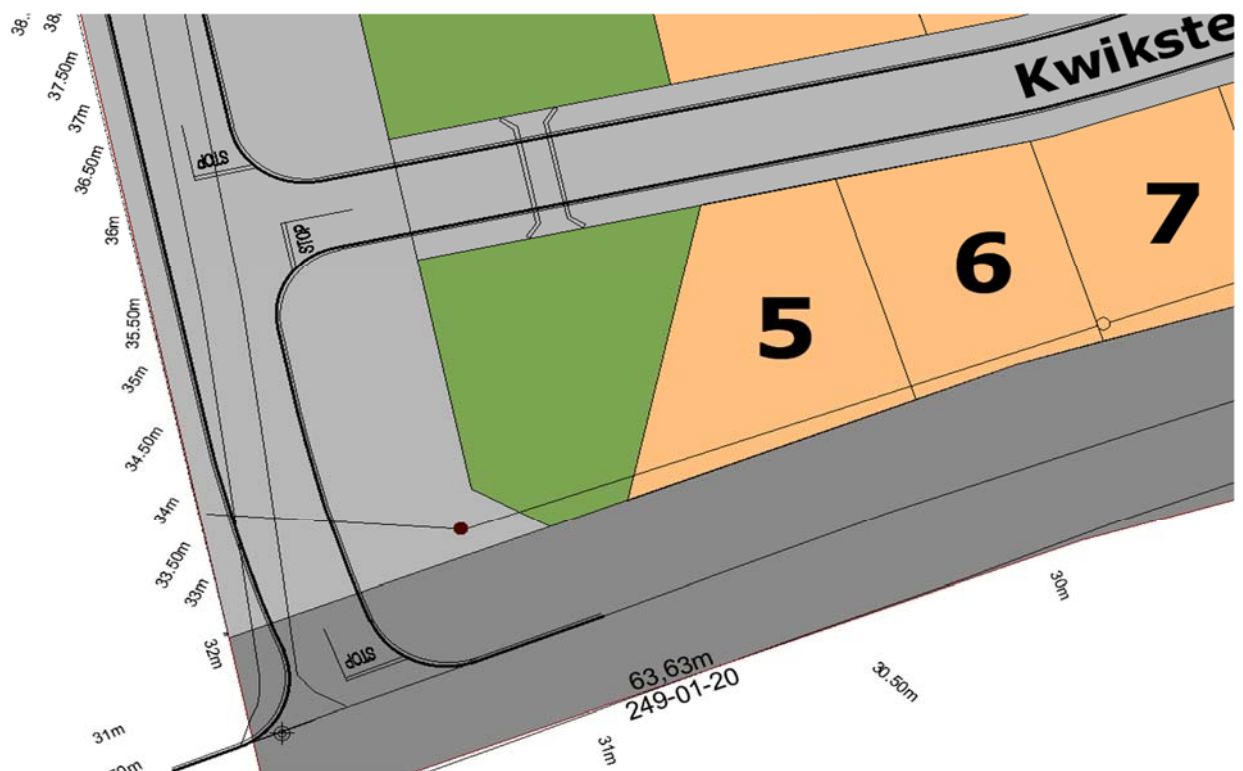


Figure 11-1 - Road Marking Layout

- 1.5. Due to the steep gradient along Tarentaal Street, it is recommended that the weight of construction vehicles be limited to 8 tonne per axle and that no articulated trucks be allowed.
- 1.6. The proposed SDP does not make provision for any type of access control. Should this be retrofitted at a later stage, the exact position must be determined in order to allow for sufficient stacking distance between the ingress gate and Tarentaal Street.
- 1.7. All Geometric and Pavement designs within the Road reserve should be according to the standards of the road authority and must be undertaken by a professionally registered Civil Engineer.

# **ANNEXURE A**

# **SITE PHOTOGRAPHS**





# **ANNEXURE B**

# **SITE DEVELOPMENT PLAN**



3/138

2832

1/138

2/138

5131

44/129

87/129

5/138

4719/195000

1/137

35/137

47/129

37/137

5/137

124/129

RE 48/129

6066/2004001

45/129

46/129



Cell: 082 464 7871 | email: janvral@vodrail.co.za  
PROJECT

DRAWING TITLE

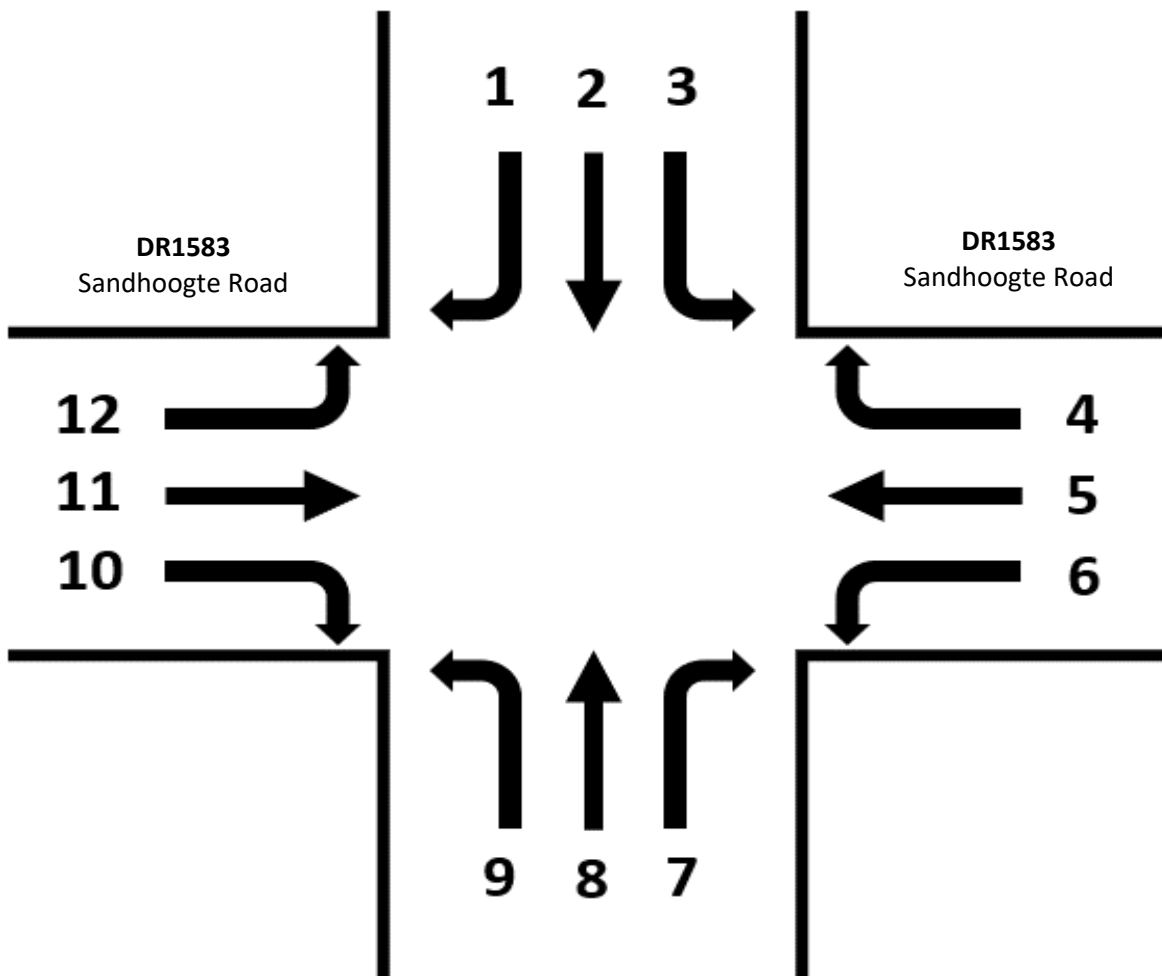
| PROJECT No.     | DWG No.      | REVISION No. | DATE OF PRINT |
|-----------------|--------------|--------------|---------------|
| ERF 2833 G BRAK | P.2          | 3            | 08.09.2023    |
| SCALE           | PROJECT DATE | DRAWN BY     | CHECKED BY    |
| NTS             | SEPT 2023    | AA           | JV            |



# **ANNEXURE C**

# **TRAFFIC VOLUMES**

DR1578 from Friemersheim



DR1578 from Tergniet

## Verkeerstelling/Traffic Count

**Projek Naam:** TIA Transand  
**Plek/Location:** Grootbrak River: Sandhoogte Rd  
**Datum/Date:** 10/05/2023  
**Teller/Counter:** JE Giewelaar



| Tyd           | DR1578 (From Friemersheim) |   |     |    |    |   | DR1583 (from Great Brak River) |   |    |   |    |   |
|---------------|----------------------------|---|-----|----|----|---|--------------------------------|---|----|---|----|---|
|               | 1                          |   | 2   |    | 3  |   | 4                              |   | 5  |   | 6  |   |
|               | L                          | S | L   | S  | L  | S | L                              | S | L  | S | L  | S |
| 06:00 - 06:15 | 0                          | 0 | 13  | 0  | 1  | 0 | 0                              | 0 | 0  | 0 | 1  | 0 |
| 06:15 - 06:30 | 0                          | 0 | 29  | 0  | 1  | 0 | 0                              | 0 | 1  | 0 | 1  | 0 |
| 06:30 - 06:45 | 3                          | 0 | 58  | 1  | 1  | 0 | 3                              | 0 | 1  | 0 | 1  | 0 |
| 06:45 - 07:00 | 3                          | 0 | 80  | 5  | 5  | 0 | 6                              | 0 | 2  | 0 | 2  | 0 |
| 07:00 - 07:15 | 4                          | 0 | 107 | 6  | 5  | 0 | 8                              | 0 | 3  | 0 | 5  | 0 |
| 07:15 - 07:30 | 4                          | 0 | 132 | 7  | 6  | 0 | 8                              | 0 | 3  | 0 | 9  | 0 |
| 07:30 - 07:45 | 5                          | 0 | 150 | 9  | 9  | 0 | 10                             | 0 | 4  | 0 | 15 | 0 |
| 07:45 - 08:00 | 5                          | 0 | 165 | 10 | 10 | 1 | 11                             | 0 | 4  | 0 | 19 | 0 |
| 08:00 - 08:15 | 6                          | 0 | 173 | 11 | 10 | 1 | 12                             | 0 | 4  | 0 | 21 | 0 |
| 08:15 - 08:30 | 6                          | 0 | 187 | 13 | 11 | 1 | 12                             | 0 | 4  | 0 | 24 | 0 |
| 08:30 - 08:45 | 6                          | 0 | 196 | 14 | 11 | 1 | 13                             | 0 | 4  | 0 | 25 | 0 |
| 08:45 - 09:00 | 9                          | 1 | 207 | 18 | 13 | 1 | 13                             | 0 | 4  | 0 | 27 | 0 |
| 09:00 - 09:15 | 9                          | 2 | 219 | 22 | 17 | 1 | 14                             | 0 | 5  | 0 | 30 | 1 |
| 09:15 - 09:30 | 10                         | 2 | 227 | 29 | 17 | 1 | 14                             | 0 | 5  | 1 | 33 | 1 |
| 09:30 - 09:45 | 10                         | 2 | 240 | 30 | 17 | 1 | 15                             | 0 | 5  | 1 | 35 | 1 |
| 09:45 - 10:00 | 10                         | 2 | 250 | 34 | 17 | 1 | 16                             | 0 | 5  | 1 | 39 | 1 |
| 10:00 - 10:15 | 11                         | 2 | 262 | 38 | 17 | 1 | 16                             | 0 | 5  | 1 | 41 | 1 |
| 10:15 - 10:30 | 14                         | 2 | 271 | 43 | 19 | 1 | 17                             | 0 | 8  | 1 | 43 | 1 |
| 10:30 - 10:45 | 15                         | 2 | 281 | 49 | 20 | 1 | 20                             | 0 | 9  | 1 | 46 | 1 |
| 10:45 - 11:00 | 15                         | 2 | 295 | 53 | 20 | 1 | 21                             | 0 | 9  | 2 | 46 | 1 |
| 11:00 - 11:15 | 16                         | 2 | 307 | 56 | 20 | 1 | 22                             | 0 | 9  | 3 | 56 | 1 |
| 11:15 - 11:30 | 18                         | 2 | 320 | 62 | 20 | 1 | 23                             | 0 | 9  | 3 | 57 | 1 |
| 11:30 - 11:45 | 18                         | 3 | 330 | 67 | 21 | 1 | 24                             | 0 | 9  | 4 | 58 | 2 |
| 11:45 - 12:00 | 19                         | 3 | 343 | 72 | 23 | 1 | 24                             | 0 | 9  | 4 | 60 | 2 |
| 12:00 - 12:15 | 20                         | 3 | 360 | 74 | 26 | 1 | 24                             | 0 | 10 | 4 | 63 | 2 |
| 12:15 - 12:30 | 24                         | 3 | 375 | 78 | 26 | 1 | 24                             | 0 | 10 | 4 | 63 | 2 |
| 12:30 - 12:45 | 25                         | 3 | 380 | 80 | 26 | 1 | 25                             | 0 | 11 | 4 | 66 | 2 |
| 12:45 - 13:00 | 27                         | 3 | 400 | 84 | 26 | 1 | 27                             | 0 | 11 | 4 | 69 | 2 |
| 13:00 - 13:15 | 28                         | 4 | 413 | 85 | 26 | 1 | 28                             | 0 | 12 | 5 | 72 | 2 |

|               |    |   |     |     |    |   |    |   |    |   |     |   |
|---------------|----|---|-----|-----|----|---|----|---|----|---|-----|---|
| 13:15 - 13:30 | 28 | 5 | 430 | 86  | 26 | 1 | 28 | 0 | 12 | 5 | 74  | 2 |
| 13:30 - 13:45 | 28 | 5 | 451 | 91  | 26 | 1 | 30 | 0 | 16 | 6 | 76  | 2 |
| 13:45 - 14:00 | 29 | 5 | 460 | 96  | 26 | 1 | 31 | 0 | 17 | 6 | 77  | 2 |
| 14:00 - 14:15 | 29 | 5 | 477 | 102 | 27 | 2 | 31 | 0 | 18 | 6 | 80  | 2 |
| 14:15 - 14:30 | 30 | 5 | 494 | 105 | 27 | 2 | 33 | 0 | 18 | 6 | 81  | 2 |
| 14:30 - 14:45 | 31 | 5 | 508 | 113 | 29 | 2 | 34 | 0 | 19 | 6 | 81  | 2 |
| 14:45 - 15:00 | 33 | 5 | 525 | 117 | 30 | 2 | 35 | 0 | 19 | 6 | 87  | 2 |
| 15:00 - 15:15 | 33 | 5 | 539 | 121 | 31 | 2 | 35 | 0 | 19 | 6 | 88  | 2 |
| 15:15 - 15:30 | 34 | 5 | 549 | 130 | 33 | 2 | 36 | 0 | 21 | 7 | 89  | 2 |
| 15:30 - 15:45 | 35 | 5 | 563 | 132 | 33 | 2 | 37 | 0 | 22 | 7 | 93  | 2 |
| 15:45 - 16:00 | 36 | 5 | 567 | 138 | 35 | 2 | 37 | 0 | 23 | 7 | 94  | 2 |
| 16:00 - 16:15 | 36 | 5 | 581 | 143 | 36 | 2 | 37 | 0 | 23 | 7 | 103 | 2 |
| 16:15 - 16:30 | 36 | 5 | 598 | 146 | 36 | 2 | 40 | 0 | 24 | 7 | 110 | 2 |
| 16:30 - 16:45 | 38 | 5 | 619 | 151 | 39 | 2 | 44 | 0 | 26 | 7 | 115 | 2 |
| 16:45 - 17:00 | 38 | 5 | 635 | 151 | 40 | 2 | 45 | 0 | 27 | 7 | 123 | 2 |
| 17:00 - 17:15 | 39 | 5 | 669 | 154 | 44 | 2 | 45 | 0 | 28 | 7 | 129 | 2 |
| 17:15 - 17:30 | 40 | 5 | 691 | 155 | 45 | 2 | 46 | 0 | 28 | 7 | 132 | 2 |
| 17:30 - 17:45 | 40 | 5 | 706 | 156 | 47 | 2 | 46 | 0 | 28 | 7 | 137 | 2 |
| 17:45 - 18:00 | 40 | 5 | 710 | 157 | 47 | 2 | 47 | 0 | 28 | 7 | 140 | 2 |



## Verkeerstelling/Traffic Count

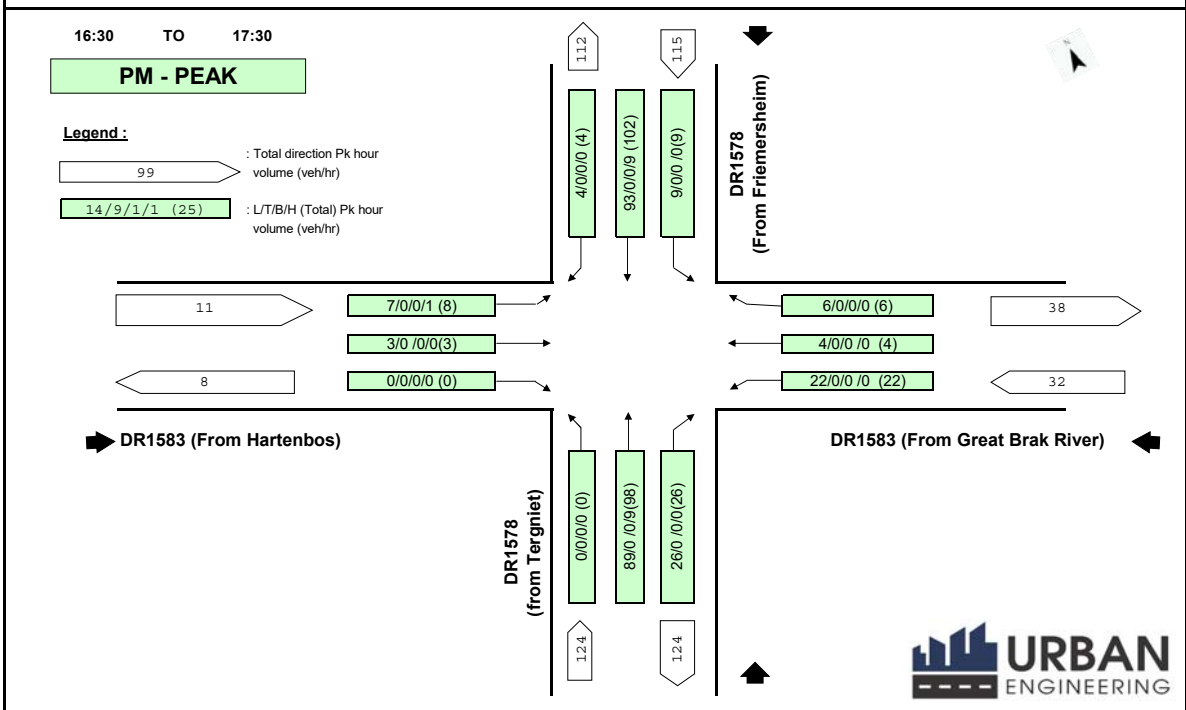
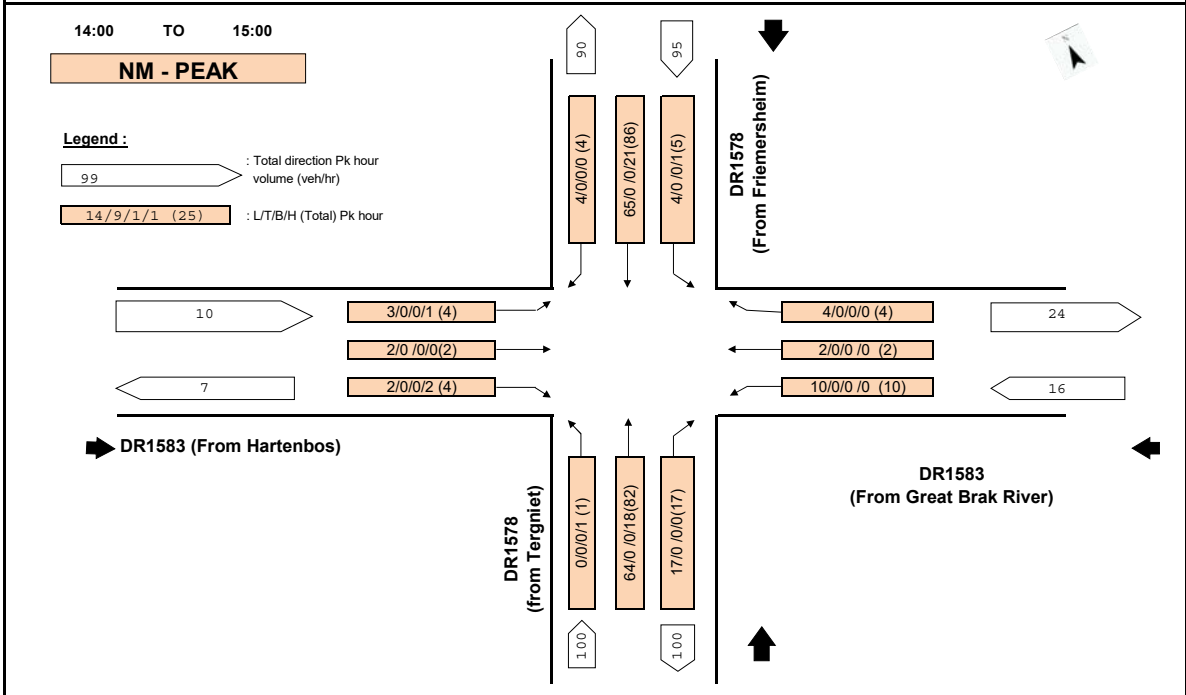
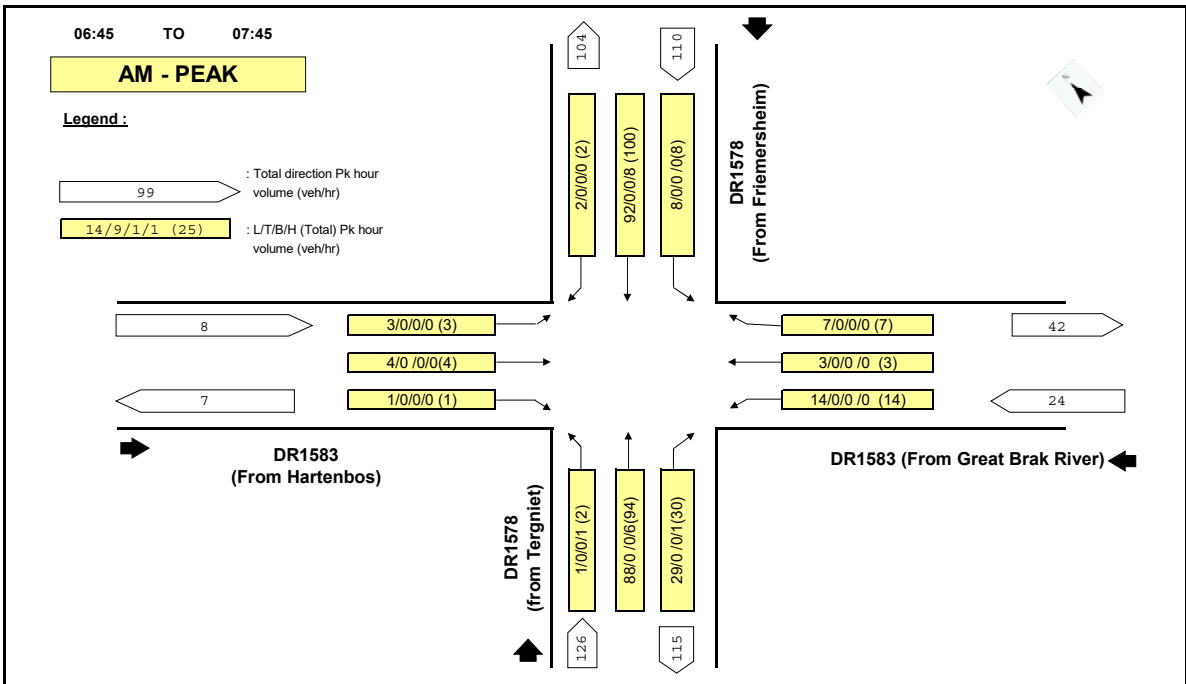
**Projek Naam:** TIA Transand  
**Plek/Location:** Grootbrak River: Sandhoogte Rd  
**Datum/Date:** 10/05/2023  
**Teller/Counter:** JE Giewelaar

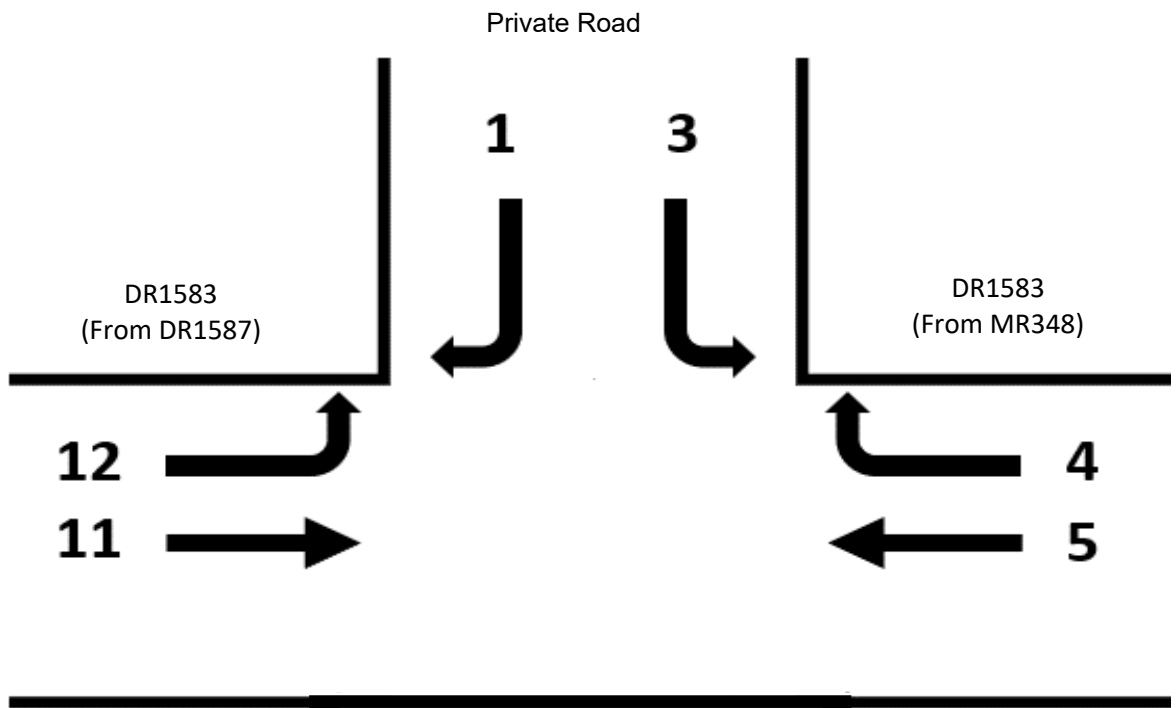


| Tyd           | DR1578 (From Tergniet) |   |     |    |   |    | DR1583 (From Hartenbos) |    |    |   |    |   |
|---------------|------------------------|---|-----|----|---|----|-------------------------|----|----|---|----|---|
|               | 7                      |   | 8   |    | 9 |    | 10                      |    | 11 |   | 12 |   |
|               | L                      | S | L   | S  | L | S  | L                       | S  | L  | S | L  | S |
| 06:00 - 06:15 | 0                      | 0 | 3   | 0  | 0 | 0  | 0                       | 0  | 1  | 0 | 0  | 0 |
| 06:15 - 06:30 | 1                      | 0 | 14  | 0  | 0 | 0  | 0                       | 0  | 1  | 0 | 0  | 0 |
| 06:30 - 06:45 | 2                      | 0 | 31  | 0  | 0 | 0  | 0                       | 0  | 1  | 0 | 0  | 0 |
| 06:45 - 07:00 | 5                      | 0 | 49  | 1  | 0 | 0  | 1                       | 0  | 2  | 0 | 1  | 0 |
| 07:00 - 07:15 | 13                     | 1 | 78  | 2  | 0 | 0  | 1                       | 0  | 3  | 0 | 1  | 0 |
| 07:15 - 07:30 | 24                     | 1 | 101 | 3  | 1 | 1  | 1                       | 0  | 5  | 0 | 2  | 0 |
| 07:30 - 07:45 | 31                     | 1 | 119 | 6  | 1 | 1  | 1                       | 0  | 5  | 0 | 3  | 0 |
| 07:45 - 08:00 | 35                     | 1 | 135 | 6  | 1 | 1  | 1                       | 1  | 5  | 0 | 6  | 1 |
| 08:00 - 08:15 | 36                     | 2 | 146 | 8  | 1 | 1  | 1                       | 1  | 5  | 0 | 6  | 1 |
| 08:15 - 08:30 | 37                     | 2 | 166 | 15 | 1 | 3  | 1                       | 1  | 5  | 0 | 6  | 1 |
| 08:30 - 08:45 | 39                     | 2 | 178 | 17 | 2 | 3  | 1                       | 2  | 5  | 1 | 6  | 1 |
| 08:45 - 09:00 | 42                     | 3 | 185 | 23 | 2 | 3  | 2                       | 2  | 5  | 1 | 8  | 2 |
| 09:00 - 09:15 | 46                     | 3 | 205 | 28 | 2 | 3  | 2                       | 3  | 6  | 1 | 8  | 2 |
| 09:15 - 09:30 | 48                     | 3 | 210 | 28 | 2 | 5  | 3                       | 3  | 6  | 1 | 8  | 2 |
| 09:30 - 09:45 | 52                     | 3 | 216 | 31 | 3 | 6  | 3                       | 5  | 6  | 1 | 11 | 2 |
| 09:45 - 10:00 | 56                     | 3 | 231 | 39 | 4 | 7  | 3                       | 6  | 6  | 2 | 13 | 3 |
| 10:00 - 10:15 | 59                     | 3 | 245 | 44 | 4 | 8  | 3                       | 7  | 6  | 2 | 15 | 3 |
| 10:15 - 10:30 | 60                     | 3 | 255 | 48 | 4 | 9  | 3                       | 8  | 7  | 2 | 16 | 3 |
| 10:30 - 10:45 | 62                     | 3 | 269 | 52 | 5 | 11 | 3                       | 9  | 8  | 2 | 16 | 3 |
| 10:45 - 11:00 | 65                     | 3 | 278 | 58 | 5 | 11 | 3                       | 10 | 10 | 2 | 16 | 4 |
| 11:00 - 11:15 | 68                     | 3 | 289 | 65 | 5 | 11 | 3                       | 10 | 10 | 2 | 16 | 4 |
| 11:15 - 11:30 | 71                     | 4 | 298 | 69 | 5 | 12 | 4                       | 11 | 10 | 3 | 17 | 5 |
| 11:30 - 11:45 | 72                     | 4 | 314 | 70 | 6 | 12 | 4                       | 13 | 10 | 3 | 20 | 5 |
| 11:45 - 12:00 | 74                     | 4 | 320 | 72 | 6 | 12 | 4                       | 13 | 11 | 3 | 23 | 5 |
| 12:00 - 12:15 | 77                     | 4 | 333 | 78 | 6 | 15 | 5                       | 13 | 11 | 4 | 24 | 5 |
| 12:15 - 12:30 | 77                     | 4 | 349 | 82 | 6 | 16 | 5                       | 15 | 12 | 4 | 24 | 5 |

|               |     |   |     |     |    |    |    |    |    |   |    |    |
|---------------|-----|---|-----|-----|----|----|----|----|----|---|----|----|
| 12:30 - 12:45 | 81  | 4 | 357 | 85  | 6  | 16 | 6  | 16 | 12 | 4 | 26 | 5  |
| 12:45 - 13:00 | 83  | 4 | 369 | 87  | 6  | 17 | 6  | 16 | 13 | 4 | 27 | 5  |
| 13:00 - 13:15 | 89  | 4 | 379 | 91  | 6  | 19 | 6  | 17 | 13 | 5 | 27 | 6  |
| 13:15 - 13:30 | 92  | 4 | 391 | 98  | 6  | 19 | 6  | 18 | 13 | 6 | 28 | 6  |
| 13:30 - 13:45 | 95  | 4 | 406 | 101 | 7  | 19 | 6  | 19 | 13 | 6 | 30 | 7  |
| 13:45 - 14:00 | 102 | 4 | 416 | 104 | 8  | 19 | 6  | 19 | 14 | 6 | 30 | 7  |
| 14:00 - 14:15 | 106 | 4 | 428 | 109 | 8  | 19 | 6  | 20 | 14 | 6 | 31 | 7  |
| 14:15 - 14:30 | 111 | 4 | 444 | 114 | 8  | 20 | 8  | 20 | 14 | 6 | 32 | 7  |
| 14:30 - 14:45 | 115 | 4 | 467 | 118 | 8  | 20 | 8  | 21 | 15 | 6 | 32 | 8  |
| 14:45 - 15:00 | 119 | 4 | 480 | 122 | 8  | 20 | 8  | 21 | 16 | 6 | 33 | 8  |
| 15:00 - 15:15 | 124 | 4 | 500 | 125 | 10 | 21 | 8  | 21 | 17 | 6 | 34 | 9  |
| 15:15 - 15:30 | 126 | 4 | 520 | 135 | 10 | 21 | 8  | 22 | 18 | 6 | 34 | 9  |
| 15:30 - 15:45 | 129 | 4 | 526 | 139 | 10 | 21 | 9  | 22 | 18 | 6 | 35 | 9  |
| 15:45 - 16:00 | 133 | 4 | 543 | 144 | 10 | 21 | 10 | 22 | 18 | 6 | 36 | 9  |
| 16:00 - 16:15 | 139 | 4 | 565 | 147 | 10 | 21 | 10 | 22 | 18 | 6 | 36 | 9  |
| 16:15 - 16:30 | 144 | 4 | 585 | 151 | 10 | 21 | 10 | 22 | 18 | 6 | 37 | 9  |
| 16:30 - 16:45 | 151 | 4 | 596 | 151 | 10 | 21 | 10 | 22 | 19 | 6 | 38 | 9  |
| 16:45 - 17:00 | 159 | 4 | 625 | 154 | 10 | 21 | 10 | 22 | 21 | 6 | 38 | 10 |
| 17:00 - 17:15 | 165 | 4 | 647 | 155 | 10 | 21 | 10 | 22 | 21 | 6 | 42 | 10 |
| 17:15 - 17:30 | 170 | 4 | 674 | 160 | 10 | 21 | 10 | 22 | 21 | 6 | 44 | 10 |
| 17:30 - 17:45 | 172 | 4 | 687 | 160 | 10 | 21 | 10 | 22 | 21 | 6 | 45 | 10 |
| 17:45 - 18:00 | 174 | 4 | 707 | 161 | 10 | 21 | 10 | 22 | 21 | 6 | 45 | 10 |







## Verkeerstelling/Traffic Count

**Projek Naam:** TIA Transand  
**Plek/Location:** Grootbrak River: Sandhoogte Rd / Private Rd  
**Datum/Date:** 10/05/2023  
**Teller/Counter:** JE Giewelaar



| Tyd           | Private Road |   |   |   |   |   | DR1583 (from MR348) |   |     |   |   |   |
|---------------|--------------|---|---|---|---|---|---------------------|---|-----|---|---|---|
|               | 1            |   | 2 |   | 3 |   | 4                   |   | 5   |   | 6 |   |
|               | L            | S | L | S | L | S | L                   | S | L   | S | L | S |
| 06:00 - 06:15 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 2   | 0 | 0 | 0 |
| 06:15 - 06:30 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 3   | 0 | 0 | 0 |
| 06:30 - 06:45 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 5   | 0 | 0 | 0 |
| 06:45 - 07:00 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 17  | 0 | 0 | 0 |
| 07:00 - 07:15 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 30  | 0 | 0 | 0 |
| 07:15 - 07:30 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 39  | 0 | 0 | 0 |
| 07:30 - 07:45 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 48  | 0 | 0 | 0 |
| 07:45 - 08:00 | 0            | 0 | 0 | 0 | 0 | 0 | 0                   | 0 | 62  | 0 | 0 | 0 |
| 08:00 - 08:15 | 0            | 0 | 0 | 0 | 1 | 0 | 1                   | 0 | 76  | 0 | 0 | 0 |
| 08:15 - 08:30 | 0            | 0 | 0 | 0 | 1 | 0 | 1                   | 0 | 80  | 0 | 0 | 0 |
| 08:30 - 08:45 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 82  | 0 | 0 | 0 |
| 08:45 - 09:00 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 89  | 0 | 0 | 0 |
| 09:00 - 09:15 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 94  | 1 | 0 | 0 |
| 09:15 - 09:30 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 100 | 2 | 0 | 0 |
| 09:30 - 09:45 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 101 | 2 | 0 | 0 |
| 09:45 - 10:00 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 104 | 2 | 0 | 0 |
| 10:00 - 10:15 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 109 | 2 | 0 | 0 |
| 10:15 - 10:30 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 115 | 2 | 0 | 0 |
| 10:30 - 10:45 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 118 | 2 | 0 | 0 |
| 10:45 - 11:00 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 120 | 2 | 0 | 0 |
| 11:00 - 11:15 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 128 | 3 | 0 | 0 |
| 11:15 - 11:30 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 135 | 3 | 0 | 0 |
| 11:30 - 11:45 | 0            | 0 | 0 | 0 | 2 | 0 | 1                   | 0 | 138 | 4 | 0 | 0 |
| 11:45 - 12:00 | 0            | 0 | 0 | 0 | 2 | 0 | 2                   | 0 | 142 | 4 | 0 | 0 |
| 12:00 - 12:15 | 0            | 0 | 0 | 0 | 2 | 0 | 2                   | 0 | 147 | 4 | 0 | 0 |
| 12:15 - 12:30 | 0            | 0 | 0 | 0 | 2 | 0 | 2                   | 0 | 151 | 4 | 0 | 0 |
| 12:30 - 12:45 | 0            | 0 | 0 | 0 | 2 | 0 | 2                   | 0 | 154 | 4 | 0 | 0 |
| 12:45 - 13:00 | 0            | 0 | 0 | 0 | 2 | 0 | 3                   | 0 | 164 | 4 | 0 | 0 |
| 13:00 - 13:15 | 0            | 0 | 0 | 0 | 3 | 0 | 3                   | 0 | 177 | 5 | 0 | 0 |

|               |   |   |   |   |   |   |   |   |     |   |   |   |
|---------------|---|---|---|---|---|---|---|---|-----|---|---|---|
| 13:15 - 13:30 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 181 | 6 | 0 | 0 |
| 13:30 - 13:45 | 0 | 0 | 0 | 0 | 3 | 0 | 4 | 0 | 184 | 6 | 0 | 0 |
| 13:45 - 14:00 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 195 | 6 | 0 | 0 |
| 14:00 - 14:15 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 203 | 6 | 0 | 0 |
| 14:15 - 14:30 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 207 | 6 | 0 | 0 |
| 14:30 - 14:45 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 211 | 6 | 0 | 0 |
| 14:45 - 15:00 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 220 | 6 | 0 | 0 |
| 15:00 - 15:15 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 226 | 6 | 0 | 0 |
| 15:15 - 15:30 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 234 | 7 | 0 | 0 |
| 15:30 - 15:45 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 240 | 8 | 0 | 0 |
| 15:45 - 16:00 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 248 | 8 | 0 | 0 |
| 16:00 - 16:15 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 260 | 8 | 0 | 0 |
| 16:15 - 16:30 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 273 | 8 | 0 | 0 |
| 16:30 - 16:45 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 287 | 8 | 0 | 0 |
| 16:45 - 17:00 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 303 | 8 | 0 | 0 |
| 17:00 - 17:15 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 316 | 8 | 0 | 0 |
| 17:15 - 17:30 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 320 | 8 | 0 | 0 |
| 17:30 - 17:45 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 324 | 8 | 0 | 0 |
| 17:45 - 18:00 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 328 | 8 | 0 | 0 |

## Verkeerstelling/Traffic Count

**Projek Naam:** TIA Transand  
**Plek/Location:** Grootbrak River: Sandhoogte Rd / Private Rd  
**Datum/Date:** 10/05/2023  
**Teller/Counter:** JE Giewelaar

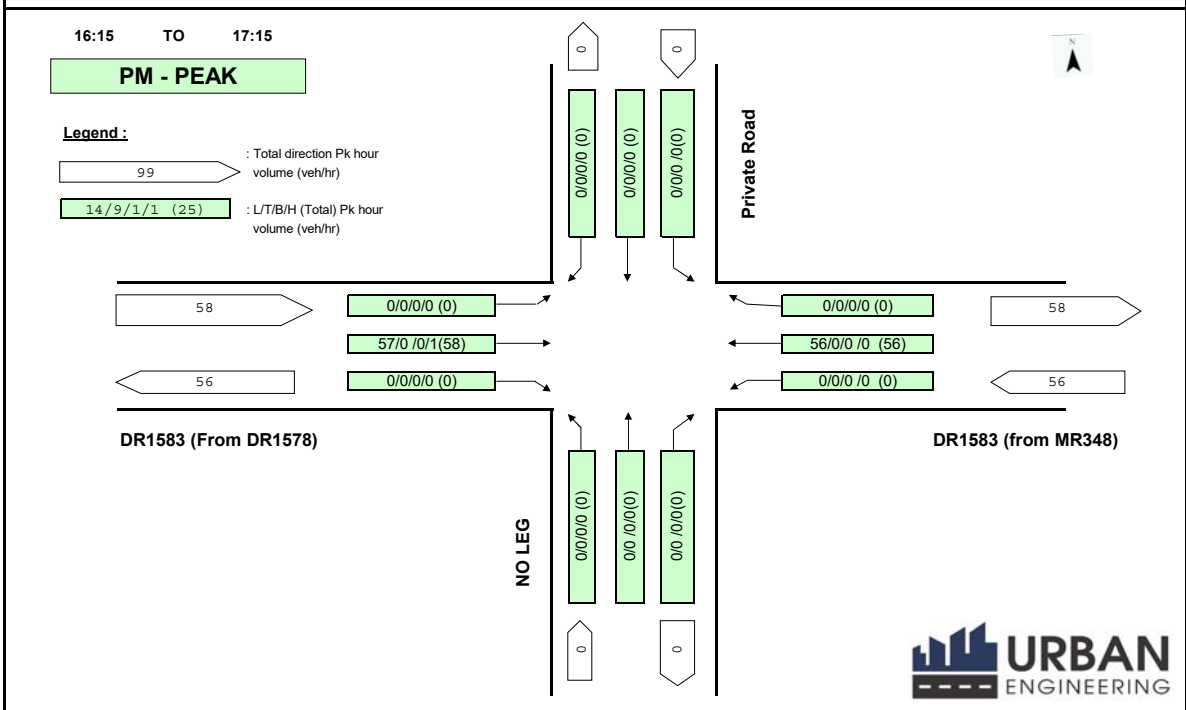
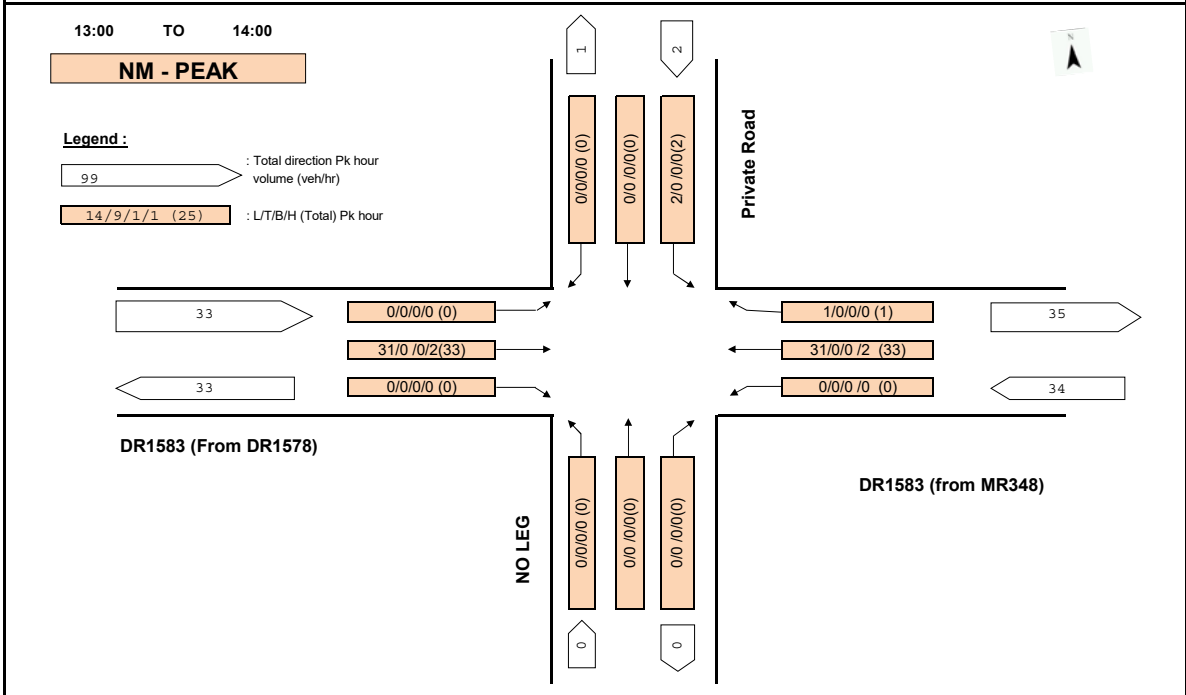
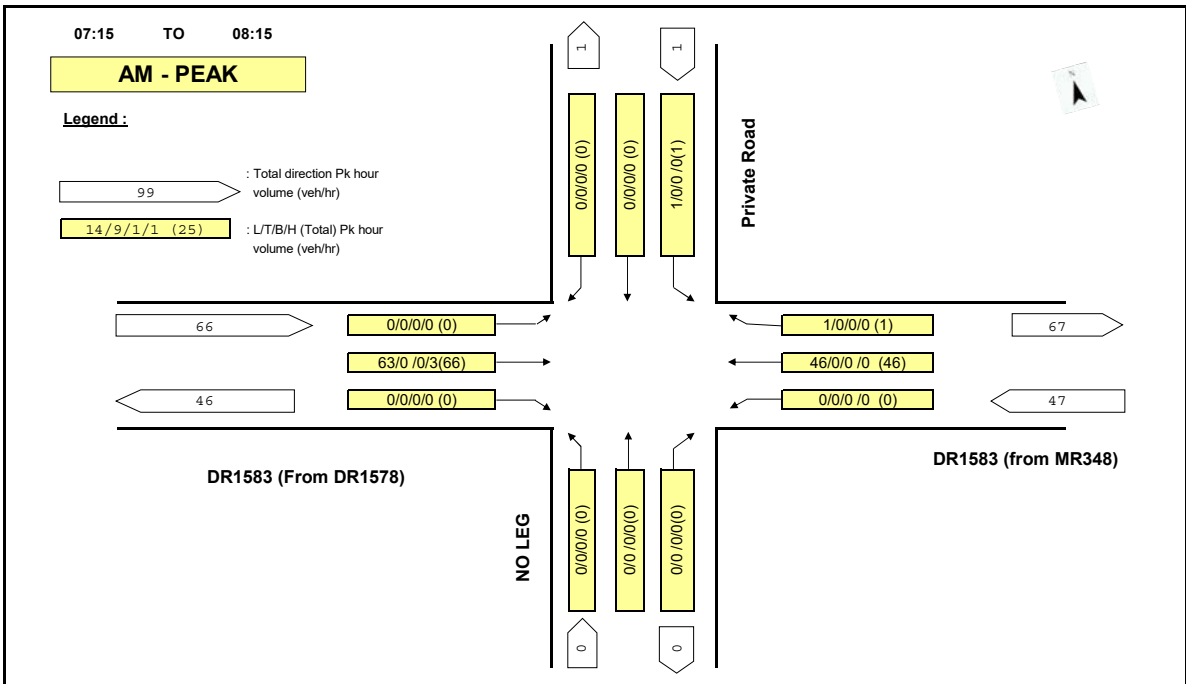


| Tyd           |   |   |   |   |   |   | DR1583 (from DR1578) |   |     |   |    |   |
|---------------|---|---|---|---|---|---|----------------------|---|-----|---|----|---|
|               | 7 |   | 8 |   | 9 |   | 10                   |   | 11  |   | 12 |   |
|               | L | S | L | S | L | S | L                    | S | L   | S | L  | S |
| 06:00 - 06:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 2   | 0 | 0  | 0 |
| 06:15 - 06:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 4   | 0 | 0  | 0 |
| 06:30 - 06:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 4   | 0 | 0  | 0 |
| 06:45 - 07:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 13  | 0 | 0  | 0 |
| 07:00 - 07:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 31  | 0 | 0  | 0 |
| 07:15 - 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 49  | 1 | 0  | 0 |
| 07:30 - 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 61  | 1 | 0  | 0 |
| 07:45 - 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 75  | 1 | 0  | 0 |
| 08:00 - 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 94  | 3 | 0  | 0 |
| 08:15 - 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 100 | 3 | 0  | 0 |
| 08:30 - 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 102 | 4 | 0  | 0 |
| 08:45 - 09:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 109 | 5 | 0  | 0 |
| 09:00 - 09:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 118 | 5 | 0  | 0 |
| 09:15 - 09:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 123 | 5 | 0  | 0 |
| 09:30 - 09:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 125 | 5 | 0  | 0 |
| 09:45 - 10:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 127 | 5 | 0  | 0 |
| 10:00 - 10:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 132 | 5 | 0  | 0 |
| 10:15 - 10:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 136 | 5 | 0  | 0 |
| 10:30 - 10:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 143 | 5 | 0  | 0 |
| 10:45 - 11:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 148 | 5 | 0  | 0 |
| 11:00 - 11:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 148 | 5 | 0  | 0 |
| 11:15 - 11:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 153 | 7 | 0  | 0 |
| 11:30 - 11:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 157 | 7 | 1  | 0 |
| 11:45 - 12:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 164 | 7 | 1  | 0 |
| 12:00 - 12:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 172 | 8 | 1  | 0 |
| 12:15 - 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0                    | 0 | 176 | 8 | 1  | 0 |

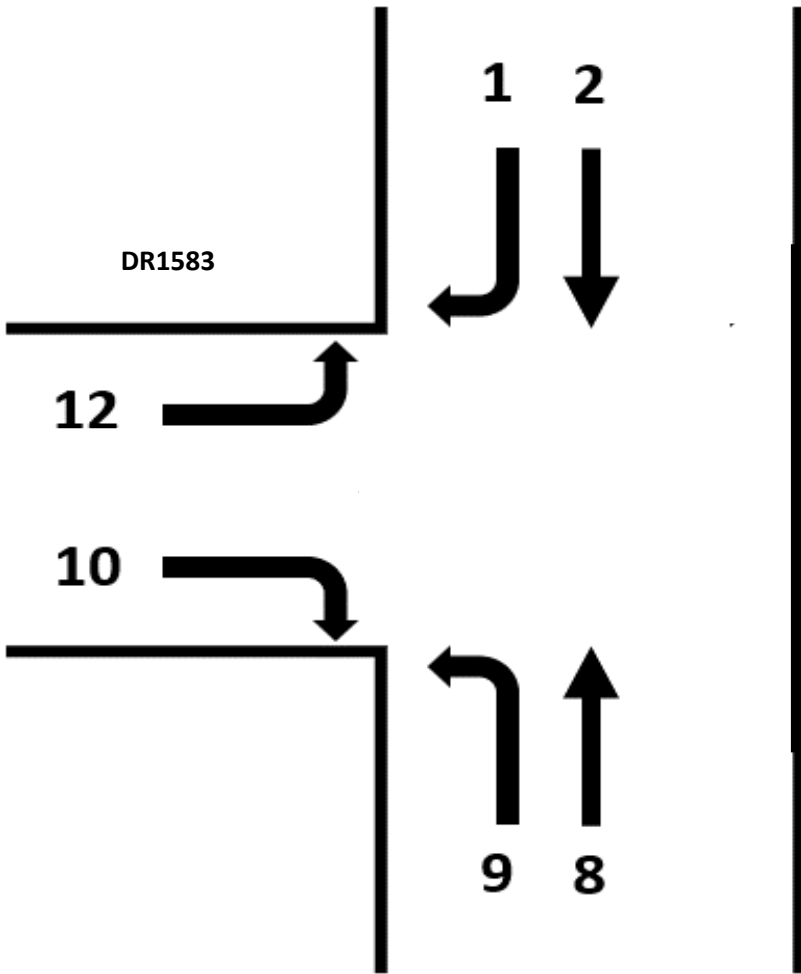


|               |   |   |   |   |   |   |   |   |   |     |    |   |   |
|---------------|---|---|---|---|---|---|---|---|---|-----|----|---|---|
| 12:30 - 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 181 | 8  | 1 | 0 |
| 12:45 - 13:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 183 | 8  | 1 | 0 |
| 13:00 - 13:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 191 | 8  | 1 | 0 |
| 13:15 - 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 198 | 9  | 1 | 0 |
| 13:30 - 13:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 201 | 9  | 1 | 0 |
| 13:45 - 14:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 214 | 10 | 1 | 0 |
| 14:00 - 14:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 220 | 10 | 1 | 0 |
| 14:15 - 14:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 228 | 10 | 1 | 0 |
| 14:30 - 14:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 237 | 10 | 1 | 0 |
| 14:45 - 15:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 241 | 10 | 2 | 0 |
| 15:00 - 15:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 10 | 2 | 0 |
| 15:15 - 15:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 261 | 10 | 2 | 0 |
| 15:30 - 15:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 264 | 10 | 2 | 0 |
| 15:45 - 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 271 | 10 | 2 | 0 |
| 16:00 - 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 282 | 10 | 2 | 0 |
| 16:15 - 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 291 | 10 | 2 | 0 |
| 16:30 - 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 305 | 11 | 2 | 0 |
| 16:45 - 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 319 | 11 | 2 | 0 |
| 17:00 - 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 339 | 11 | 2 | 0 |
| 17:15 - 17:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 344 | 11 | 2 | 0 |
| 17:30 - 17:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 347 | 11 | 2 | 0 |
| 17:45 - 18:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 347 | 11 | 2 | 0 |





MR0348



MR0348



|               |     |    |      |    |   |   |   |   |   |   |   |   |
|---------------|-----|----|------|----|---|---|---|---|---|---|---|---|
| 13:15 - 13:30 | 362 | 12 | 1272 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:30 - 13:45 | 380 | 13 | 1319 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13:45 - 14:00 | 393 | 14 | 1368 | 55 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14:00 - 14:15 | 409 | 14 | 1437 | 55 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14:15 - 14:30 | 419 | 14 | 1474 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14:30 - 14:45 | 429 | 14 | 1525 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14:45 - 15:00 | 452 | 14 | 1574 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:00 - 15:15 | 462 | 15 | 1628 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:15 - 15:30 | 472 | 16 | 1672 | 63 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:30 - 15:45 | 485 | 18 | 1707 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15:45 - 16:00 | 501 | 18 | 1753 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00 - 16:15 | 512 | 18 | 1794 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15 - 16:30 | 534 | 18 | 1854 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 - 16:45 | 557 | 18 | 1902 | 70 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 - 17:00 | 579 | 18 | 1950 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00 - 17:15 | 596 | 18 | 2005 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15 - 17:30 | 615 | 18 | 2042 | 73 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30 - 17:45 | 629 | 18 | 2079 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:45 - 18:00 | 637 | 19 | 2100 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## Verkeerstelling/Traffic Count

**Projek Naam:** TIA Transand  
**Plek/Location:** Grootbrak River: Sandhoogte Rd / Lang St  
**Datum/Date:** 10/05/2023  
**Teller/Counter:** JE Giewelaar

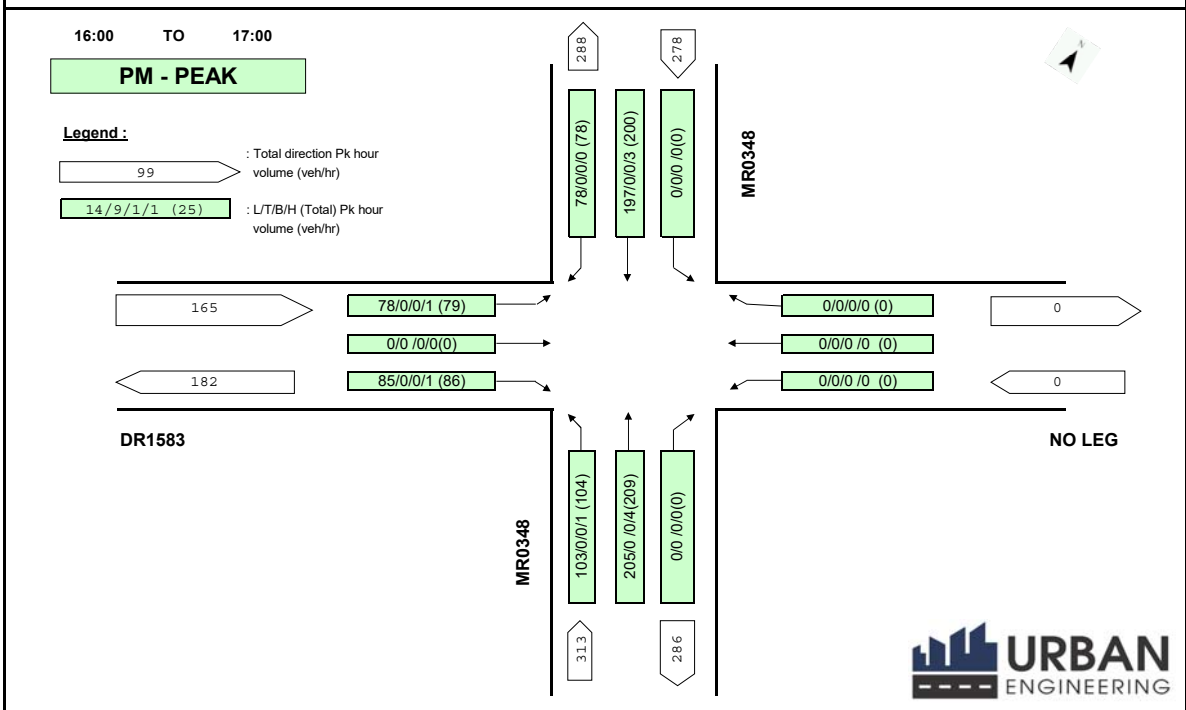
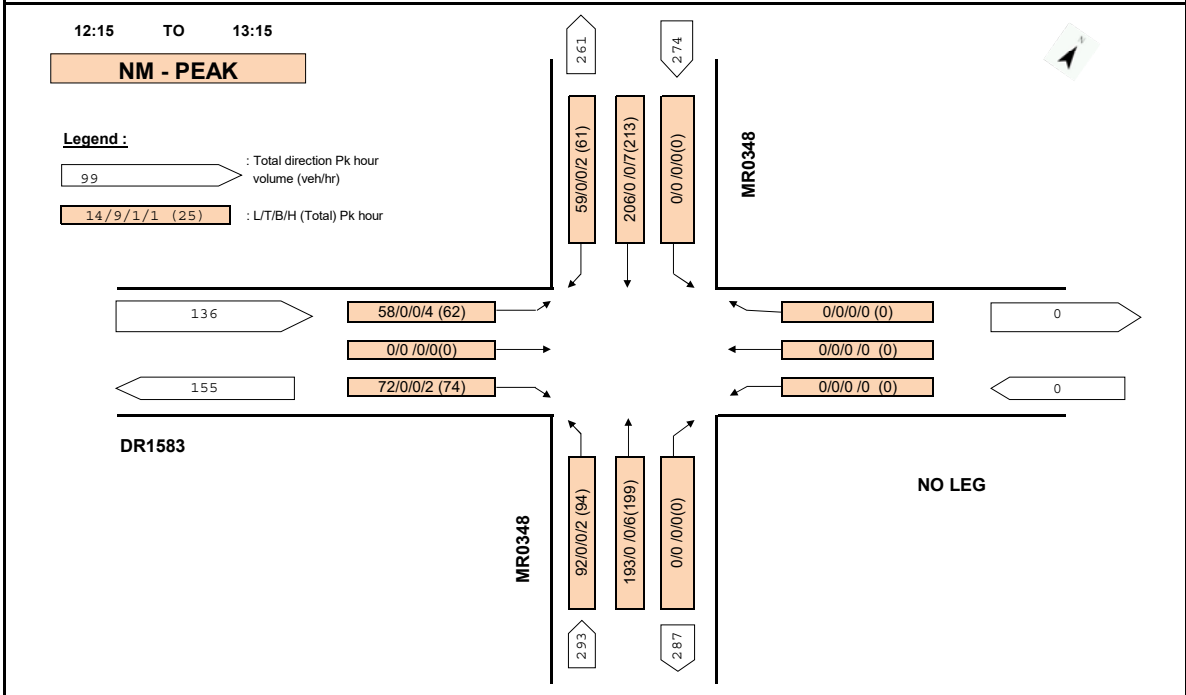
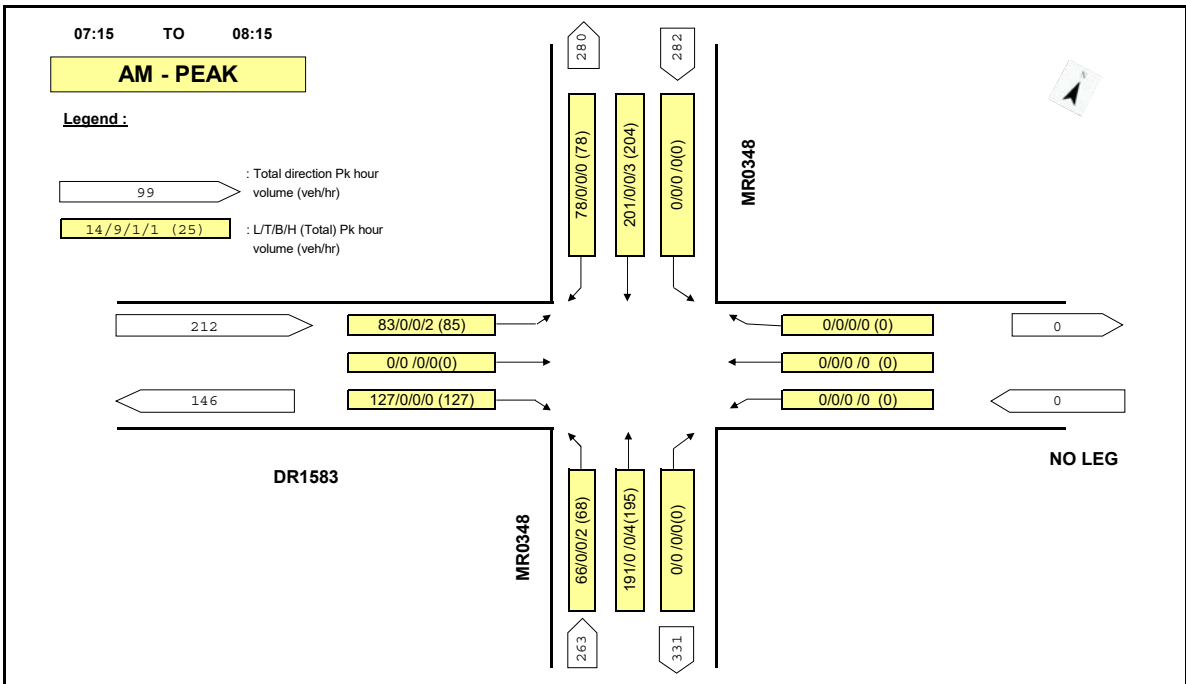


| Tyd           | MR0348 |   |      |    |     |    | DR1583 |    |    |   |     |    |
|---------------|--------|---|------|----|-----|----|--------|----|----|---|-----|----|
|               | 7      |   | 8    |    | 9   |    | 10     |    | 11 |   | 12  |    |
|               | L      | S | L    | S  | L   | S  | L      | S  | L  | S | L   | S  |
| 06:00 - 06:15 | 0      | 0 | 7    | 1  | 3   | 0  | 8      | 0  | 0  | 0 | 3   | 0  |
| 06:15 - 06:30 | 0      | 0 | 18   | 2  | 7   | 0  | 18     | 0  | 0  | 0 | 8   | 0  |
| 06:30 - 06:45 | 0      | 0 | 31   | 3  | 11  | 0  | 36     | 0  | 0  | 0 | 13  | 0  |
| 06:45 - 07:00 | 0      | 0 | 60   | 4  | 20  | 0  | 62     | 0  | 0  | 0 | 20  | 0  |
| 07:00 - 07:15 | 0      | 0 | 109  | 4  | 34  | 0  | 86     | 0  | 0  | 0 | 35  | 0  |
| 07:15 - 07:30 | 0      | 0 | 160  | 4  | 47  | 0  | 129    | 0  | 0  | 0 | 58  | 1  |
| 07:30 - 07:45 | 0      | 0 | 190  | 5  | 59  | 1  | 156    | 0  | 0  | 0 | 73  | 2  |
| 07:45 - 08:00 | 0      | 0 | 251  | 7  | 79  | 1  | 184    | 0  | 0  | 0 | 102 | 2  |
| 08:00 - 08:15 | 0      | 0 | 286  | 8  | 100 | 2  | 213    | 0  | 0  | 0 | 118 | 2  |
| 08:15 - 08:30 | 0      | 0 | 337  | 10 | 119 | 3  | 227    | 3  | 0  | 0 | 139 | 2  |
| 08:30 - 08:45 | 0      | 0 | 378  | 12 | 130 | 4  | 250    | 4  | 0  | 0 | 147 | 3  |
| 08:45 - 09:00 | 0      | 0 | 420  | 15 | 147 | 6  | 272    | 6  | 0  | 0 | 163 | 3  |
| 09:00 - 09:15 | 0      | 0 | 456  | 21 | 167 | 7  | 300    | 7  | 0  | 0 | 188 | 5  |
| 09:15 - 09:30 | 0      | 0 | 495  | 22 | 181 | 8  | 313    | 9  | 0  | 0 | 198 | 6  |
| 09:30 - 09:45 | 0      | 0 | 539  | 24 | 198 | 10 | 336    | 9  | 0  | 0 | 204 | 6  |
| 09:45 - 10:00 | 0      | 0 | 579  | 26 | 212 | 11 | 363    | 10 | 0  | 0 | 215 | 9  |
| 10:00 - 10:15 | 0      | 0 | 625  | 30 | 230 | 12 | 373    | 12 | 0  | 0 | 224 | 9  |
| 10:15 - 10:30 | 0      | 0 | 657  | 32 | 241 | 12 | 392    | 12 | 0  | 0 | 233 | 10 |
| 10:30 - 10:45 | 0      | 0 | 691  | 34 | 257 | 13 | 412    | 13 | 0  | 0 | 243 | 10 |
| 10:45 - 11:00 | 0      | 0 | 727  | 37 | 274 | 14 | 429    | 15 | 0  | 0 | 261 | 10 |
| 11:00 - 11:15 | 0      | 0 | 778  | 40 | 287 | 17 | 452    | 15 | 0  | 0 | 269 | 10 |
| 11:15 - 11:30 | 0      | 0 | 831  | 44 | 306 | 17 | 468    | 17 | 0  | 0 | 280 | 11 |
| 11:30 - 11:45 | 0      | 0 | 868  | 45 | 325 | 18 | 481    | 17 | 0  | 0 | 287 | 11 |
| 11:45 - 12:00 | 0      | 0 | 931  | 49 | 351 | 18 | 507    | 20 | 0  | 0 | 297 | 11 |
| 12:00 - 12:15 | 0      | 0 | 963  | 51 | 363 | 18 | 526    | 20 | 0  | 0 | 307 | 11 |
| 12:15 - 12:30 | 0      | 0 | 1014 | 53 | 393 | 19 | 545    | 20 | 0  | 0 | 322 | 12 |

|               |   |   |      |    |     |    |     |    |   |   |     |    |
|---------------|---|---|------|----|-----|----|-----|----|---|---|-----|----|
| 12:30 - 12:45 | 0 | 0 | 1065 | 55 | 416 | 19 | 569 | 21 | 0 | 0 | 335 | 14 |
| 12:45 - 13:00 | 0 | 0 | 1115 | 56 | 433 | 19 | 588 | 22 | 0 | 0 | 348 | 14 |
| 13:00 - 13:15 | 0 | 0 | 1156 | 57 | 455 | 20 | 598 | 22 | 0 | 0 | 365 | 15 |
| 13:15 - 13:30 | 0 | 0 | 1187 | 58 | 466 | 20 | 616 | 22 | 0 | 0 | 376 | 16 |
| 13:30 - 13:45 | 0 | 0 | 1227 | 59 | 482 | 20 | 625 | 23 | 0 | 0 | 389 | 16 |
| 13:45 - 14:00 | 0 | 0 | 1278 | 59 | 505 | 20 | 649 | 23 | 0 | 0 | 400 | 16 |
| 14:00 - 14:15 | 0 | 0 | 1338 | 59 | 526 | 20 | 671 | 23 | 0 | 0 | 415 | 16 |
| 14:15 - 14:30 | 0 | 0 | 1377 | 63 | 543 | 21 | 685 | 23 | 0 | 0 | 427 | 16 |
| 14:30 - 14:45 | 0 | 0 | 1430 | 67 | 567 | 22 | 711 | 23 | 0 | 0 | 443 | 16 |
| 14:45 - 15:00 | 0 | 0 | 1463 | 70 | 582 | 22 | 724 | 24 | 0 | 0 | 453 | 16 |
| 15:00 - 15:15 | 0 | 0 | 1507 | 71 | 613 | 22 | 750 | 24 | 0 | 0 | 466 | 17 |
| 15:15 - 15:30 | 0 | 0 | 1542 | 71 | 641 | 22 | 769 | 24 | 0 | 0 | 481 | 17 |
| 15:30 - 15:45 | 0 | 0 | 1577 | 74 | 661 | 23 | 787 | 24 | 0 | 0 | 498 | 17 |
| 15:45 - 16:00 | 0 | 0 | 1615 | 75 | 684 | 23 | 810 | 25 | 0 | 0 | 514 | 19 |
| 16:00 - 16:15 | 0 | 0 | 1660 | 77 | 705 | 23 | 828 | 25 | 0 | 0 | 535 | 20 |
| 16:15 - 16:30 | 0 | 0 | 1713 | 78 | 726 | 23 | 851 | 26 | 0 | 0 | 557 | 20 |
| 16:30 - 16:45 | 0 | 0 | 1773 | 79 | 756 | 24 | 873 | 26 | 0 | 0 | 570 | 20 |
| 16:45 - 17:00 | 0 | 0 | 1820 | 79 | 787 | 24 | 895 | 26 | 0 | 0 | 592 | 20 |
| 17:00 - 17:15 | 0 | 0 | 1843 | 80 | 815 | 24 | 917 | 26 | 0 | 0 | 603 | 20 |
| 17:15 - 17:30 | 0 | 0 | 1886 | 81 | 850 | 24 | 933 | 26 | 0 | 0 | 615 | 20 |
| 17:30 - 17:45 | 0 | 0 | 1930 | 82 | 872 | 24 | 949 | 27 | 0 | 0 | 619 | 20 |
| 17:45 - 18:00 | 0 | 0 | 1961 | 83 | 891 | 24 | 960 | 27 | 0 | 0 | 623 | 20 |

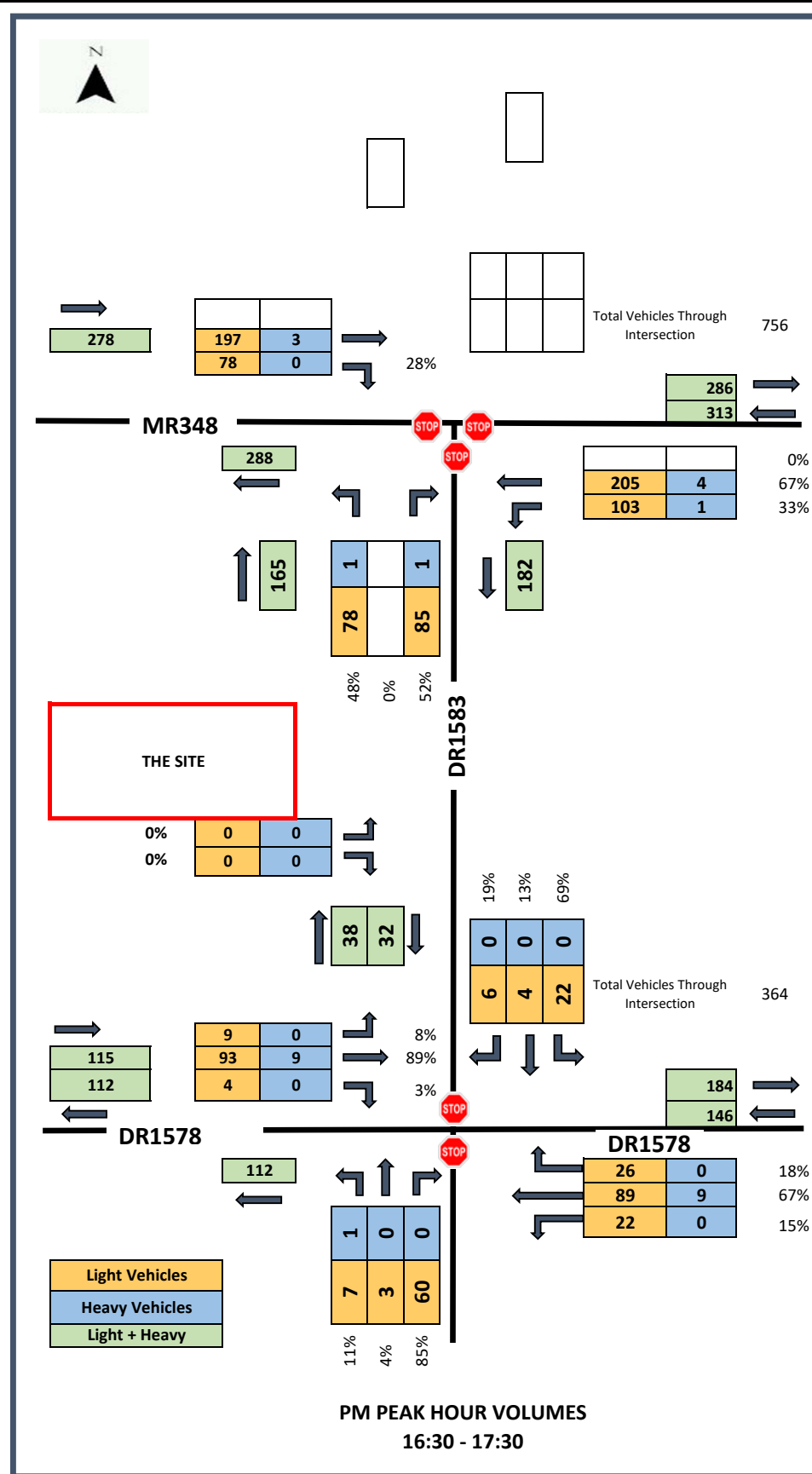
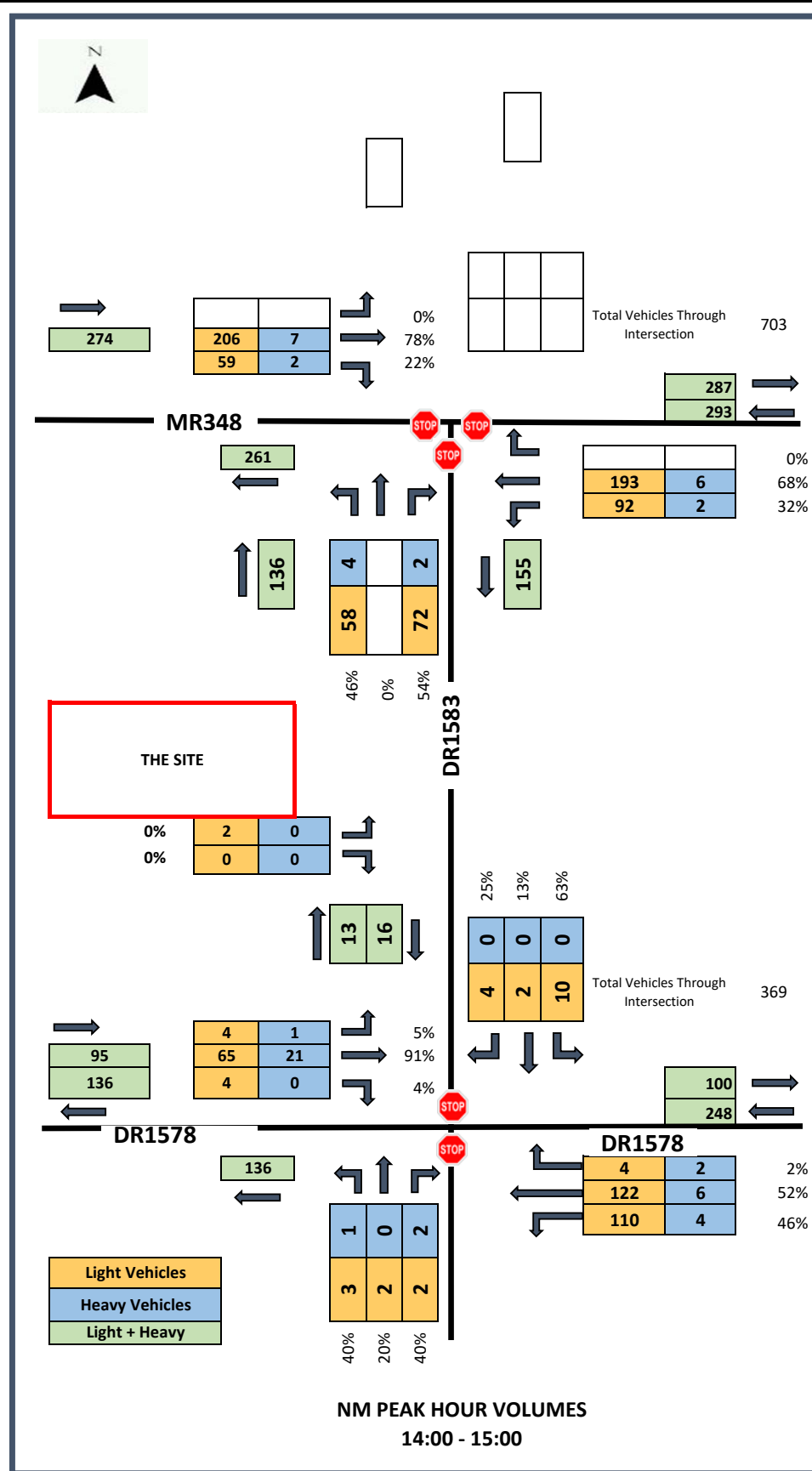
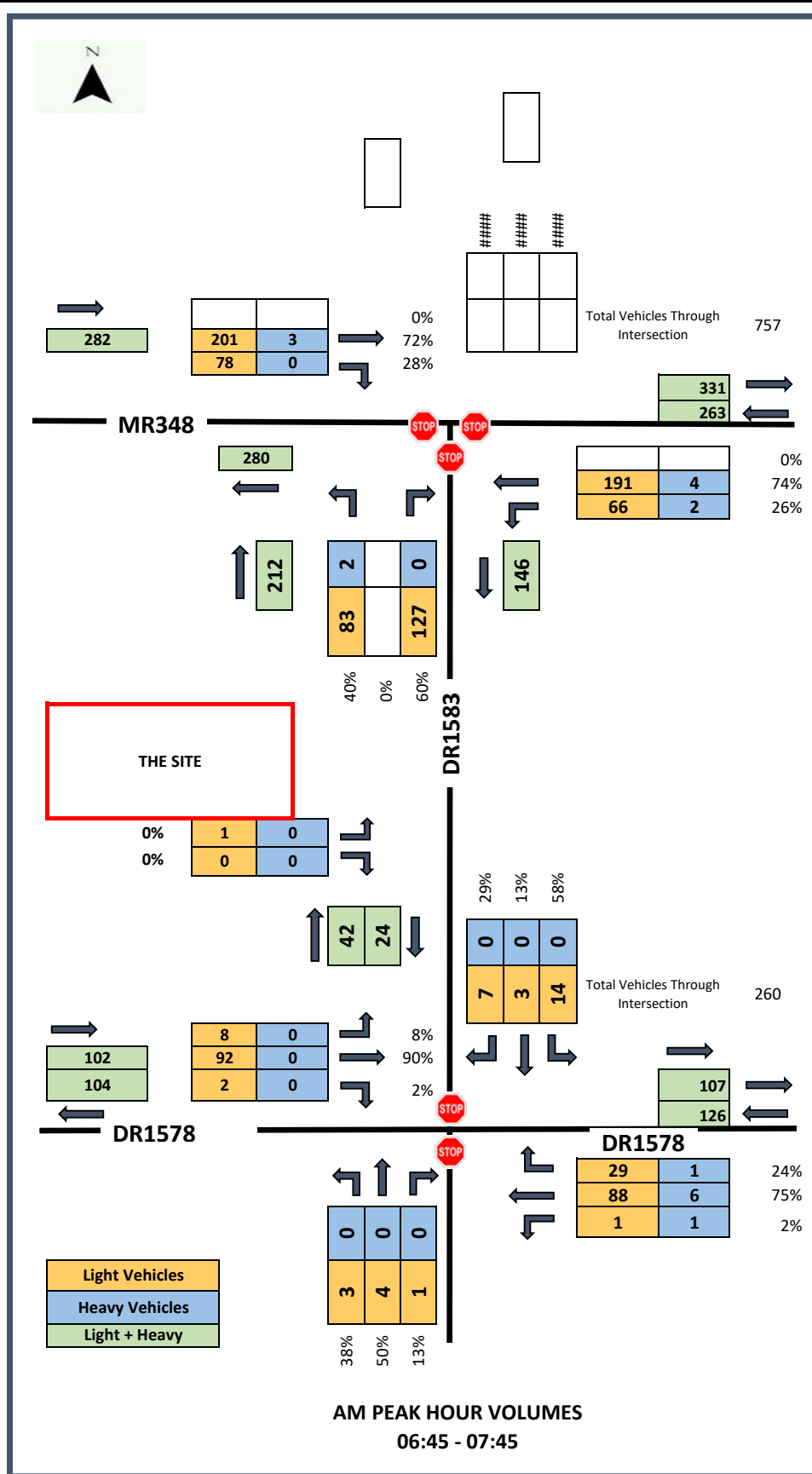






# **ANNEXURE D**

# **TRIP DISTRIBUTION**

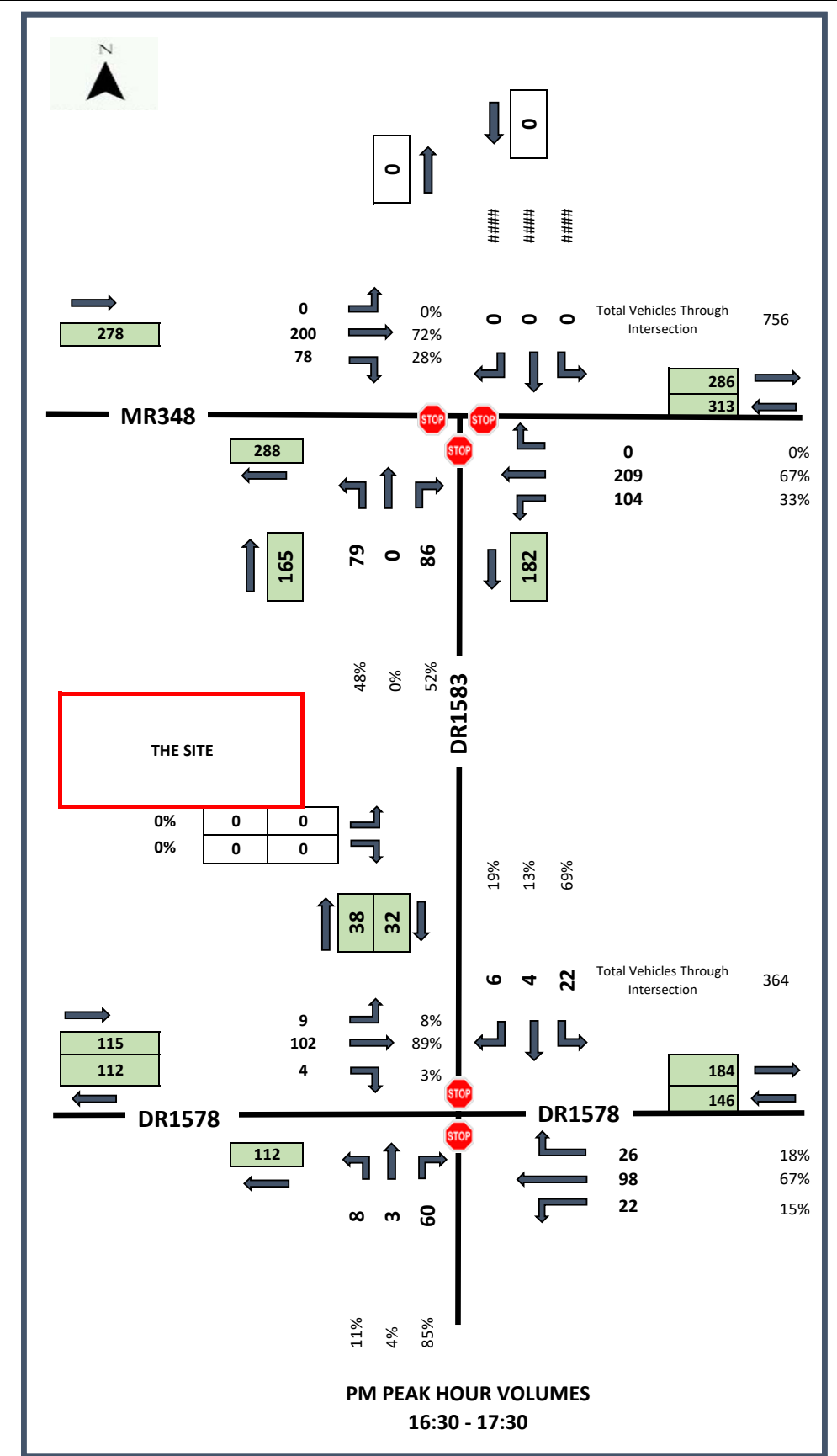
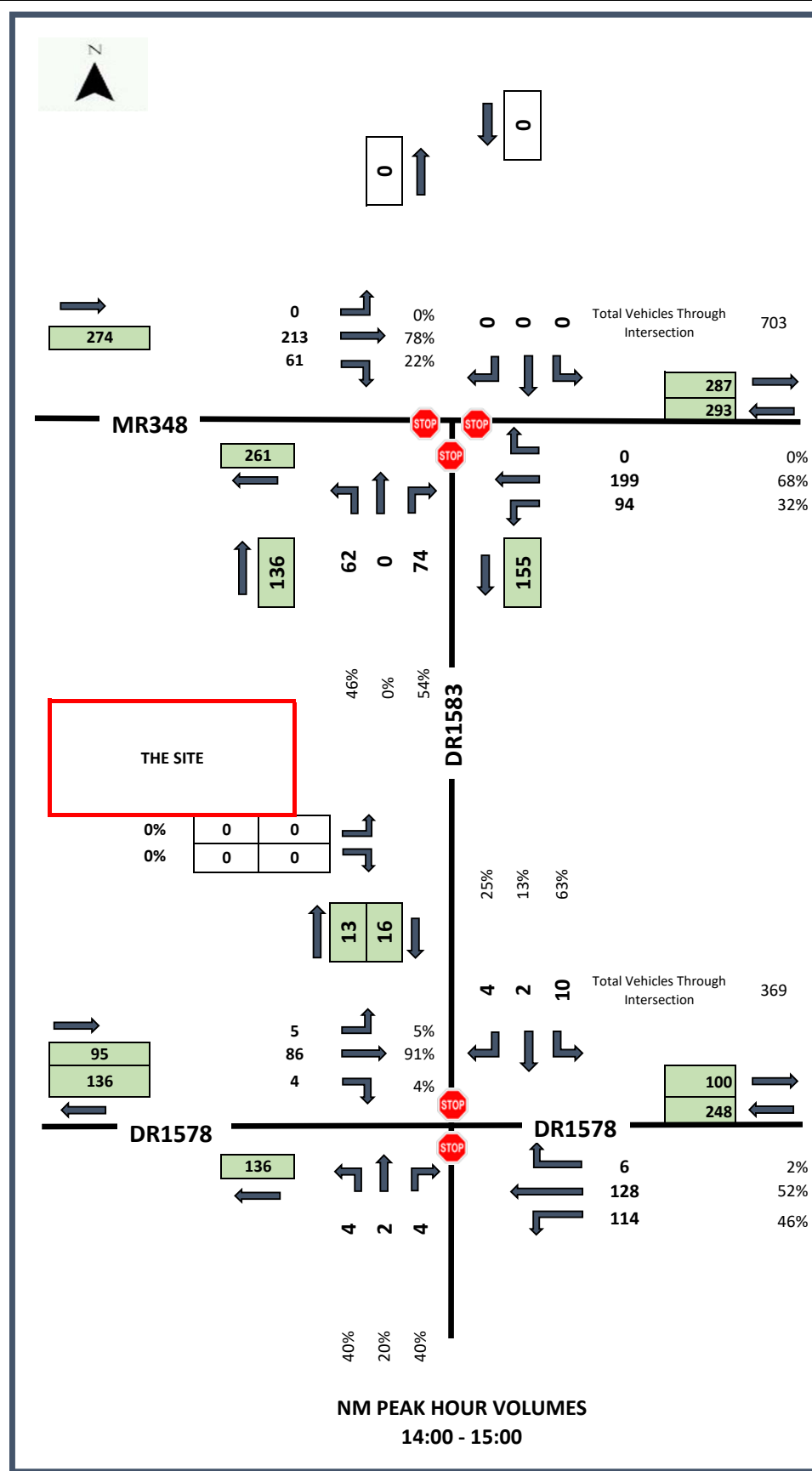
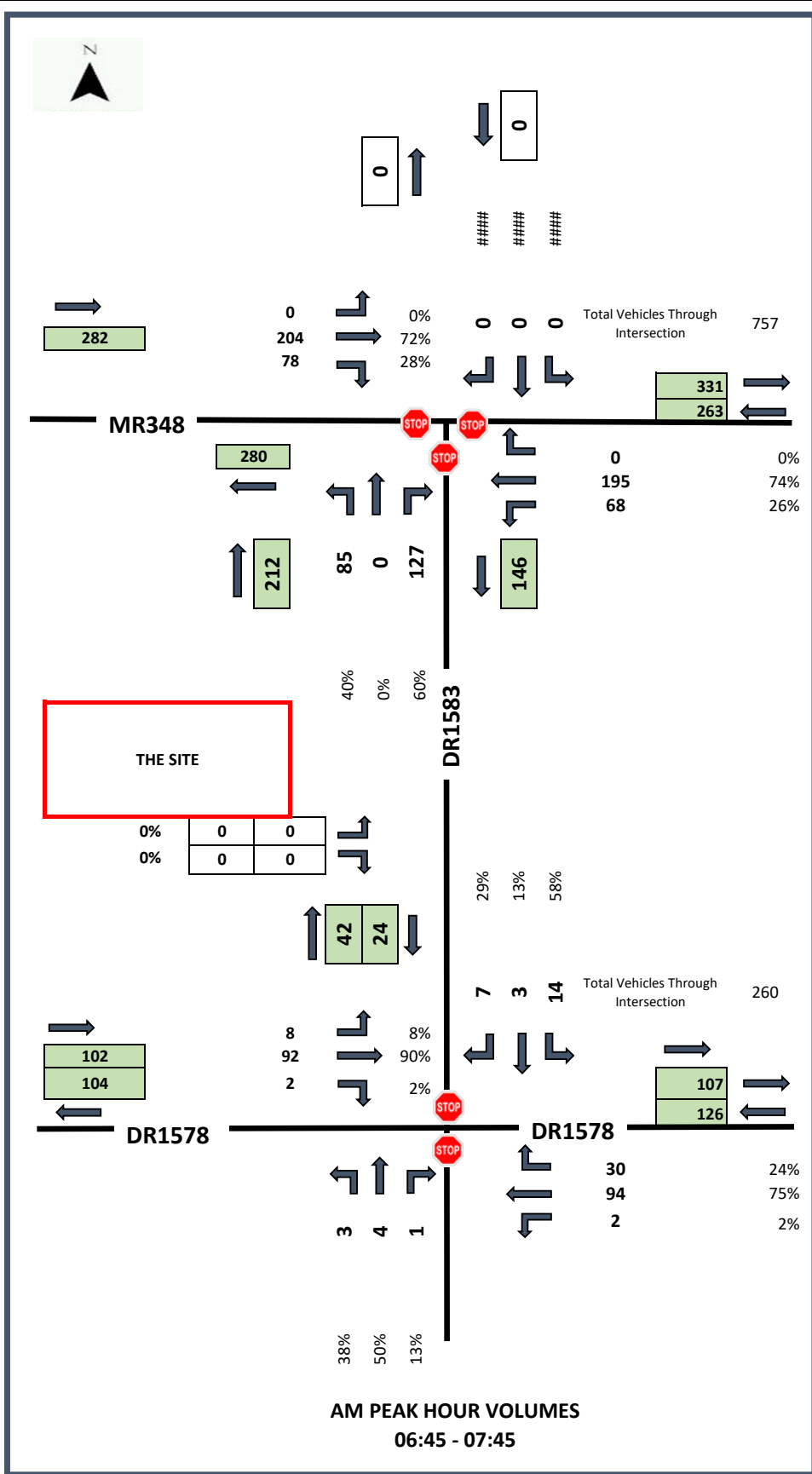


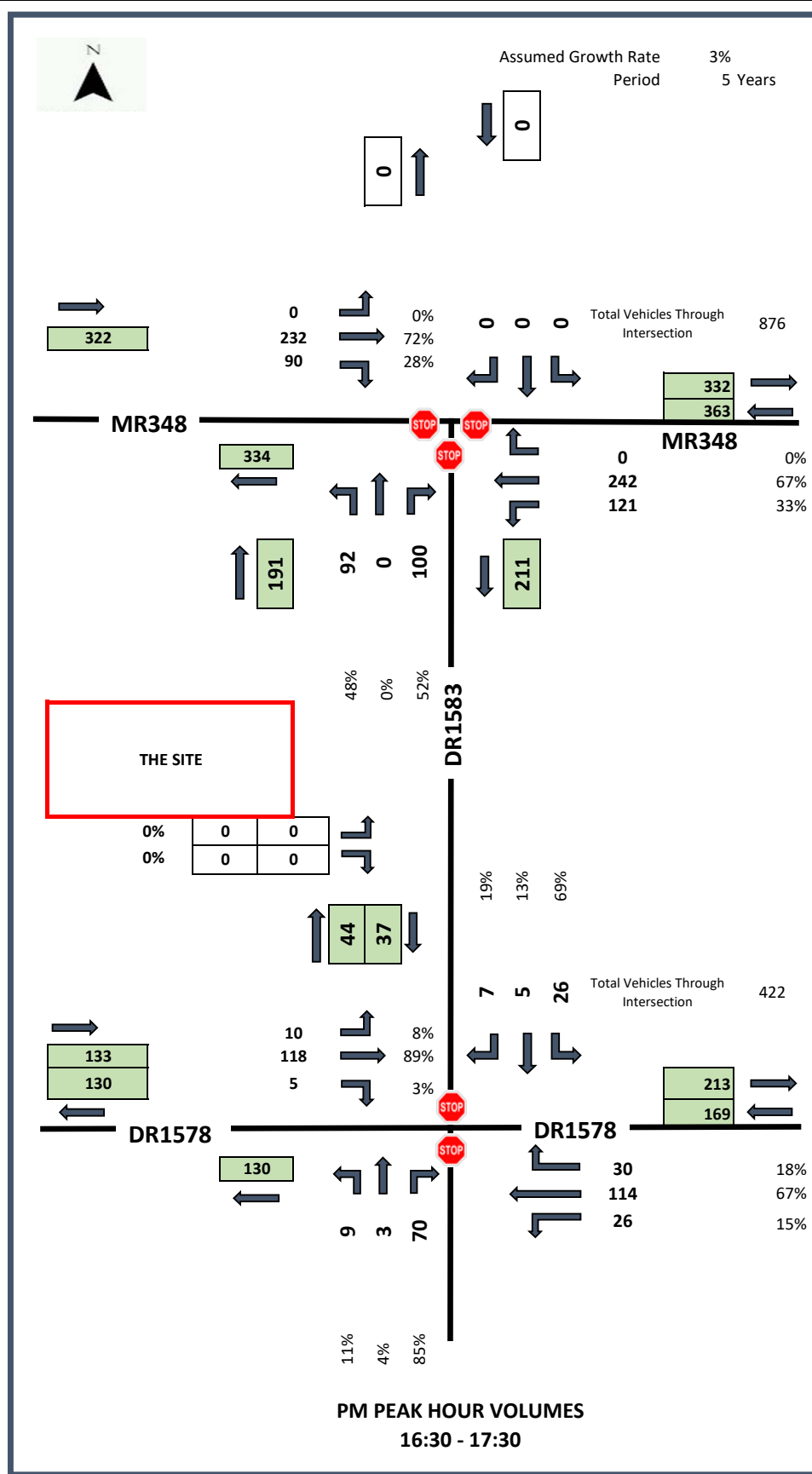
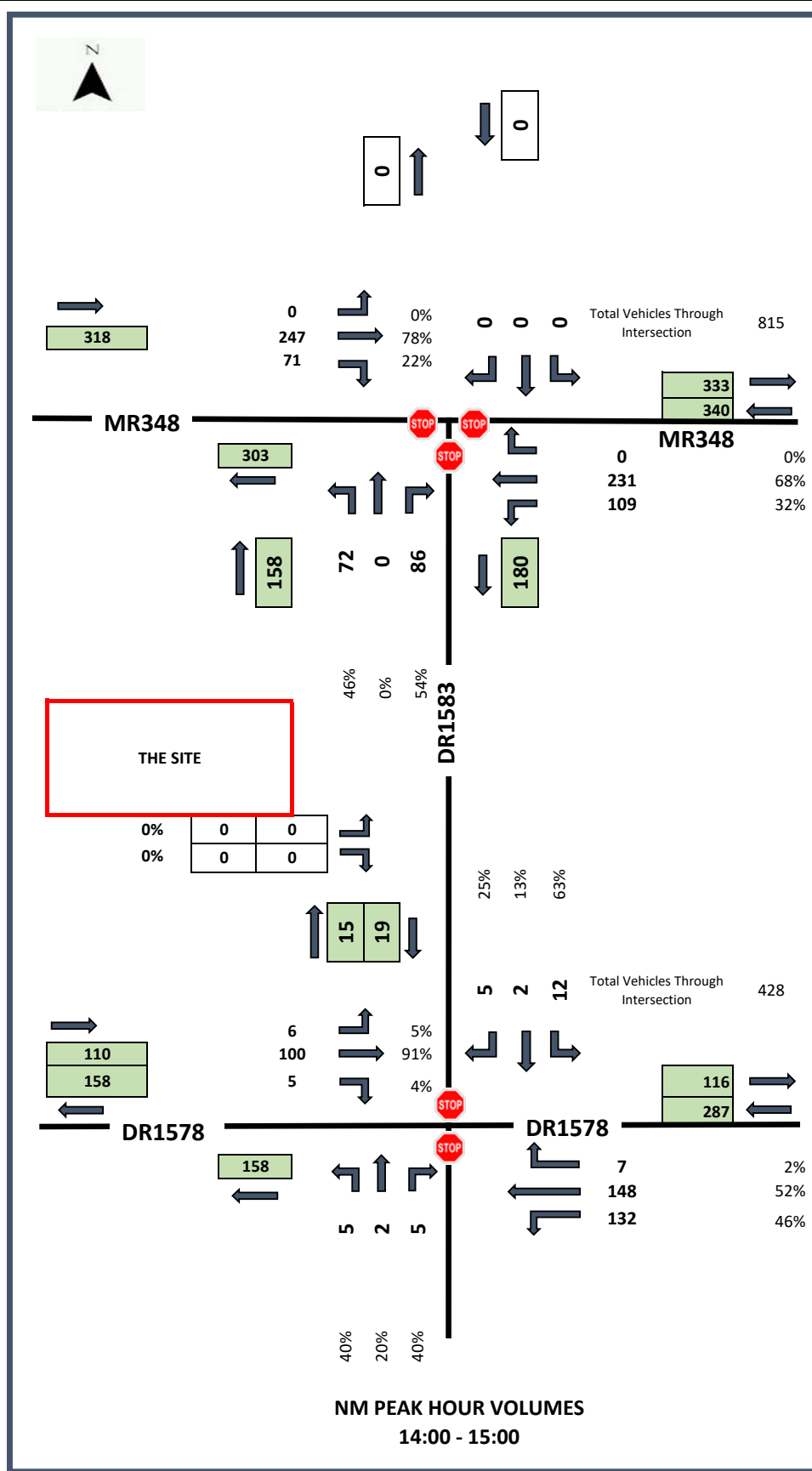
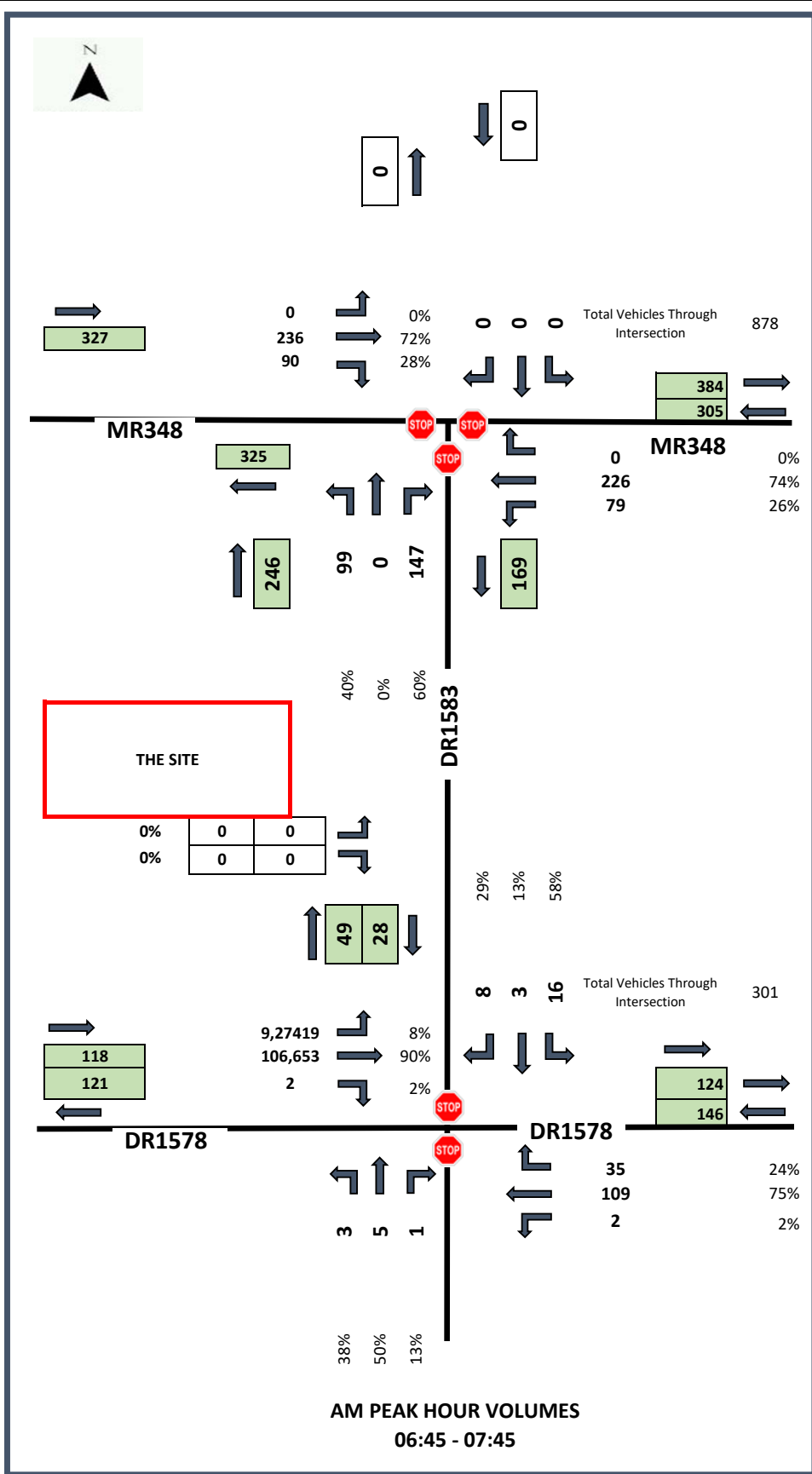
Project: **23-041 REM ERF 2833, GREAT BRAK RIVER**

Description: **PEAK HOUR VOLUMES (WEDNESDAY 05 MAY 2023)**

Legend  
 STOP CONTROLLED INTERSECTION

Title  
**FIGURE A**



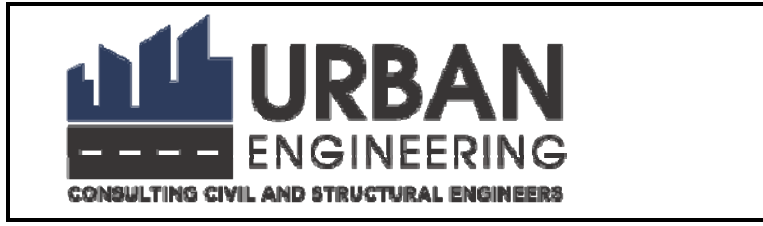
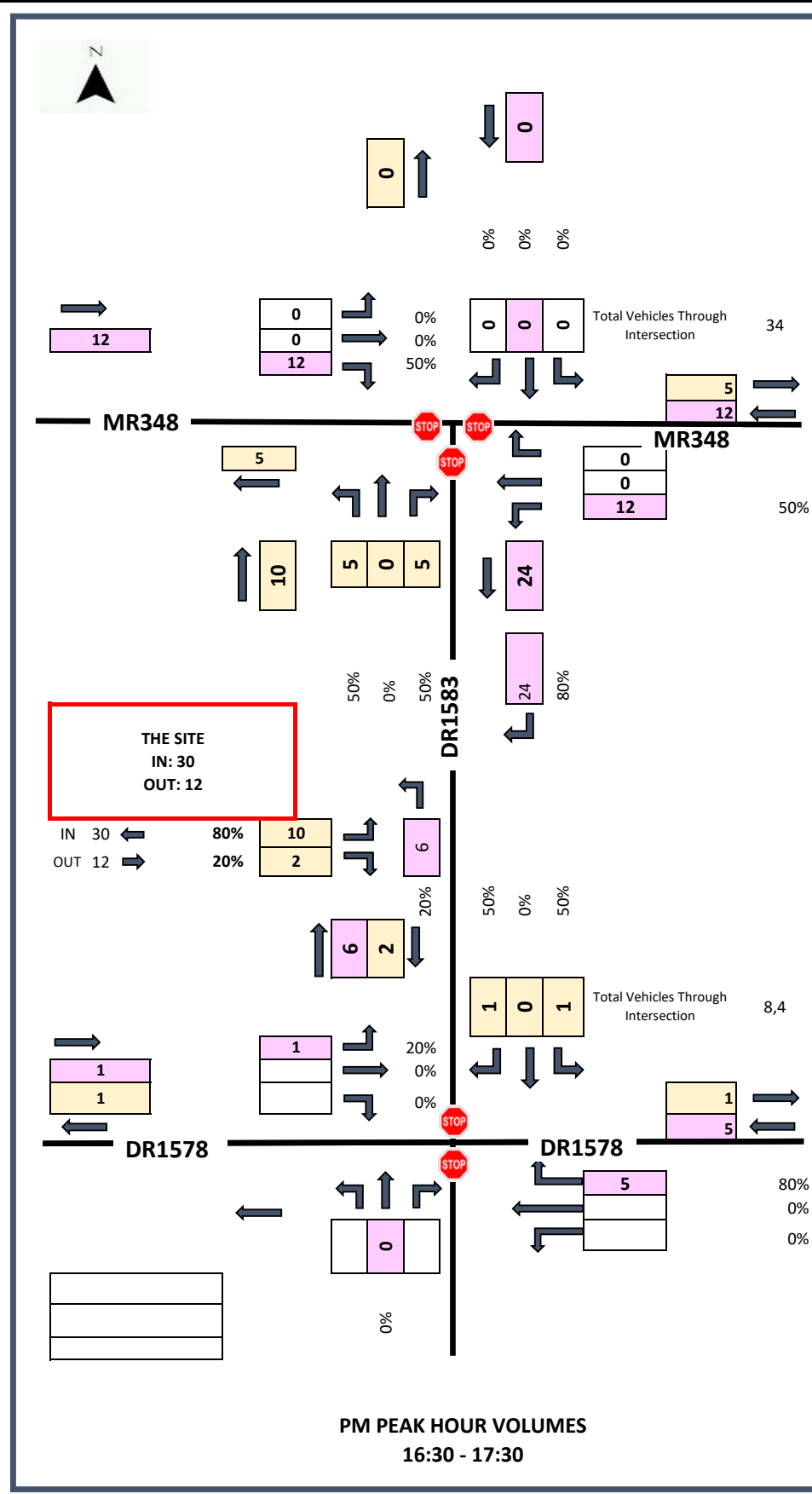
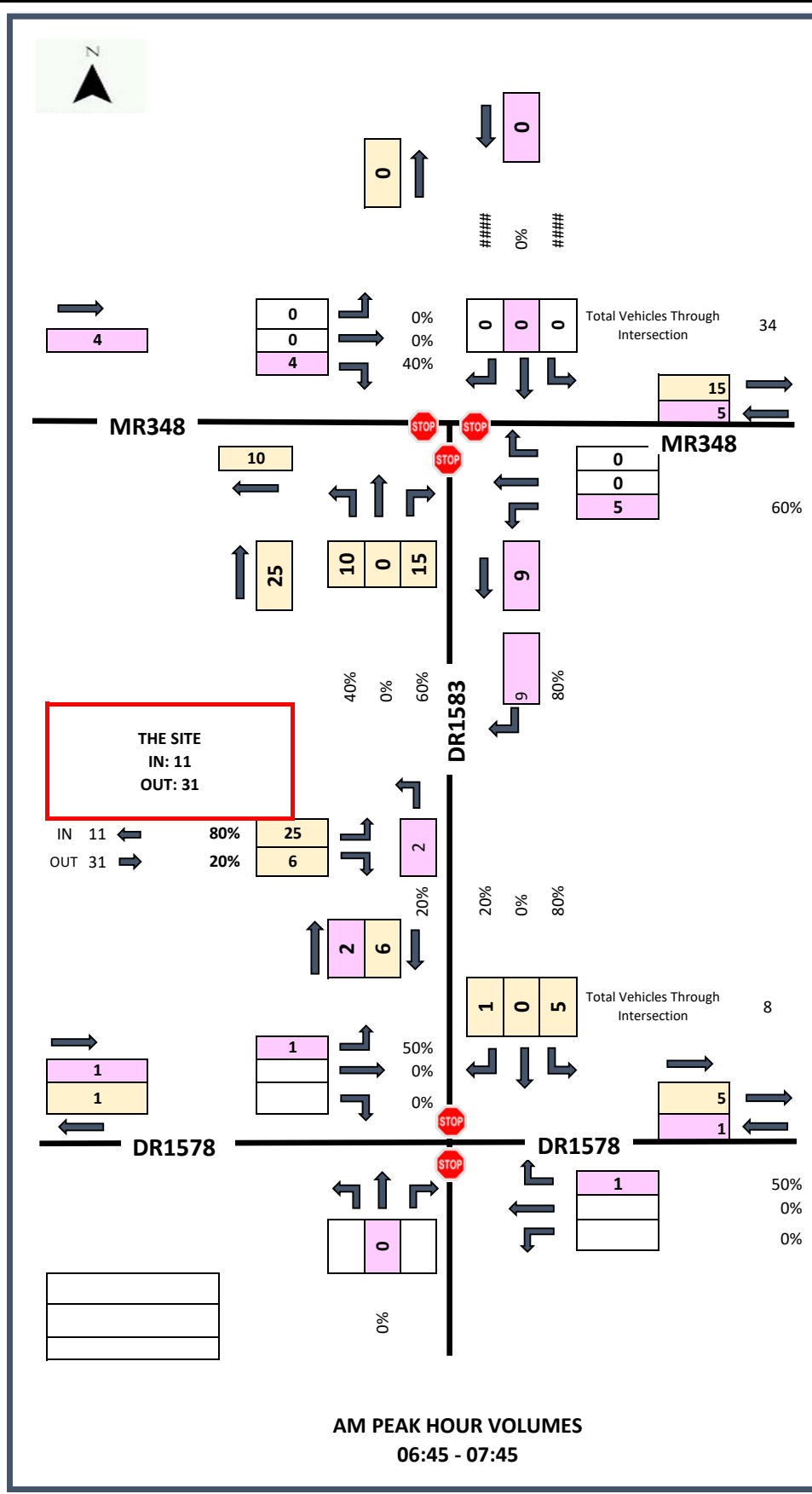


Project:  
**23-041 REM ERF 2833, GREAT BRAK RIVER**

Description:  
**ESTIMATED 2028 BACKGROUND VOLUMES (3%, 5 YEARS)**

Legend  
 STOP CONTROLLED INTERSECTION

Title  
**FIGURE C**

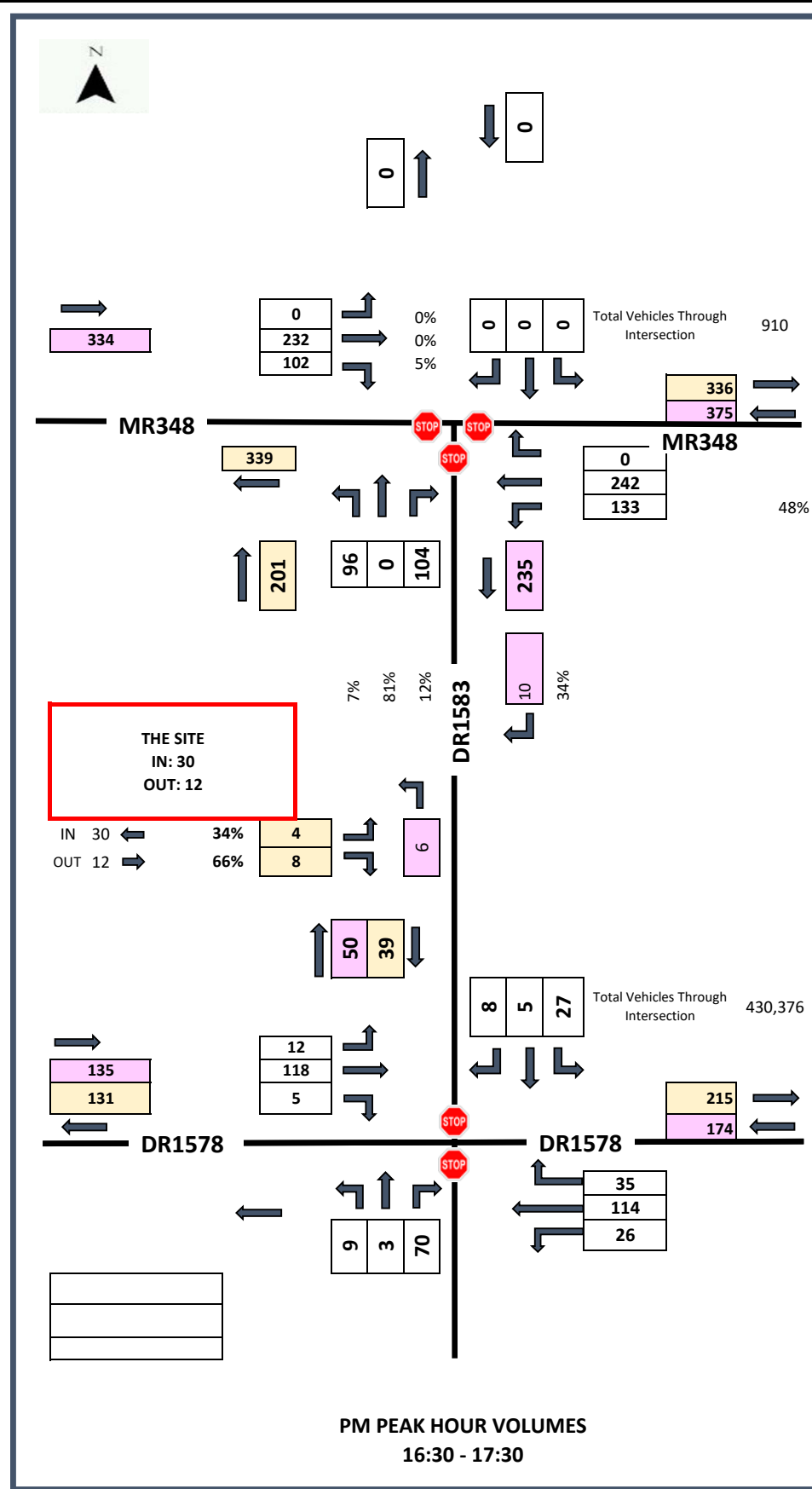
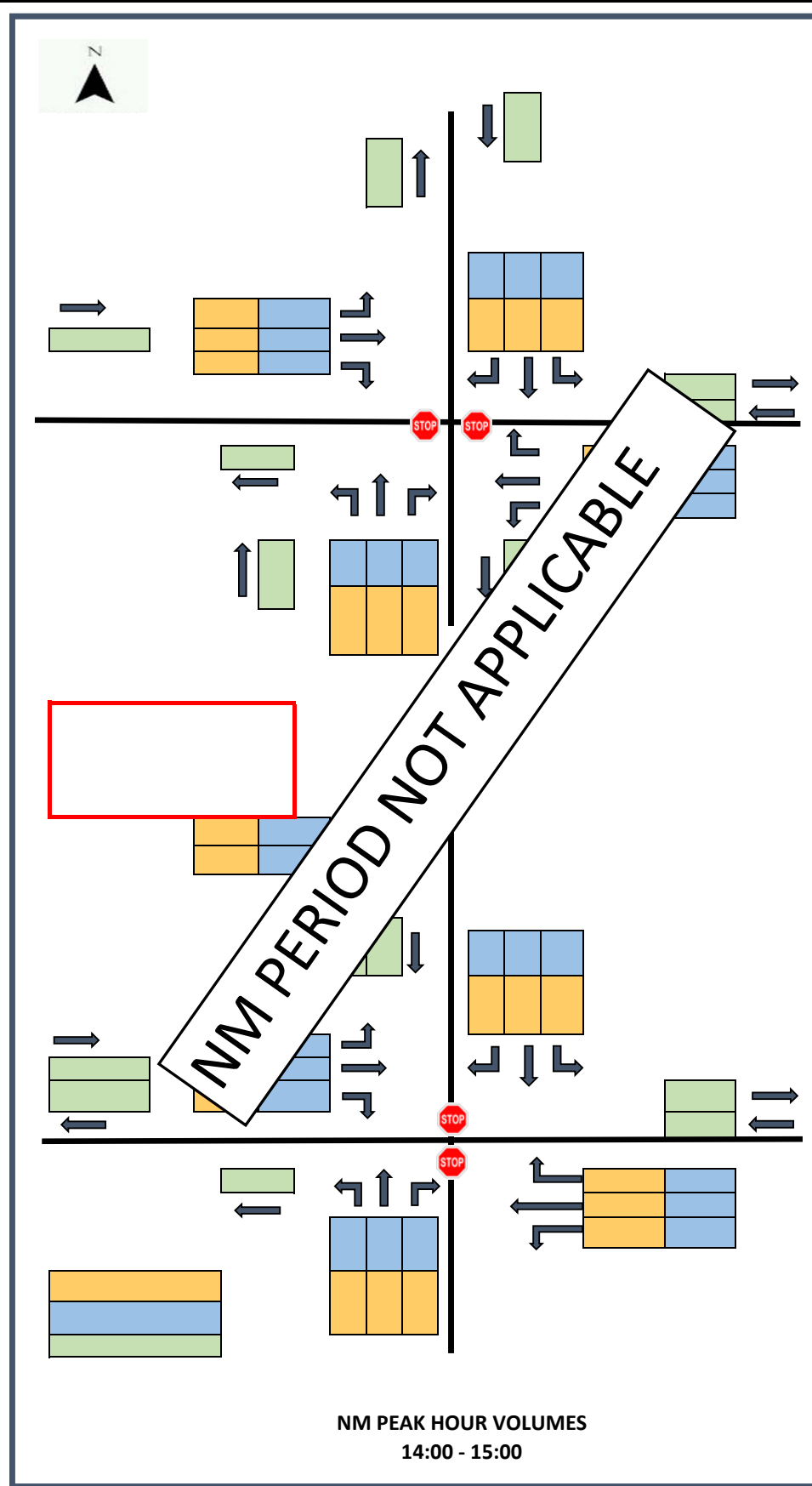
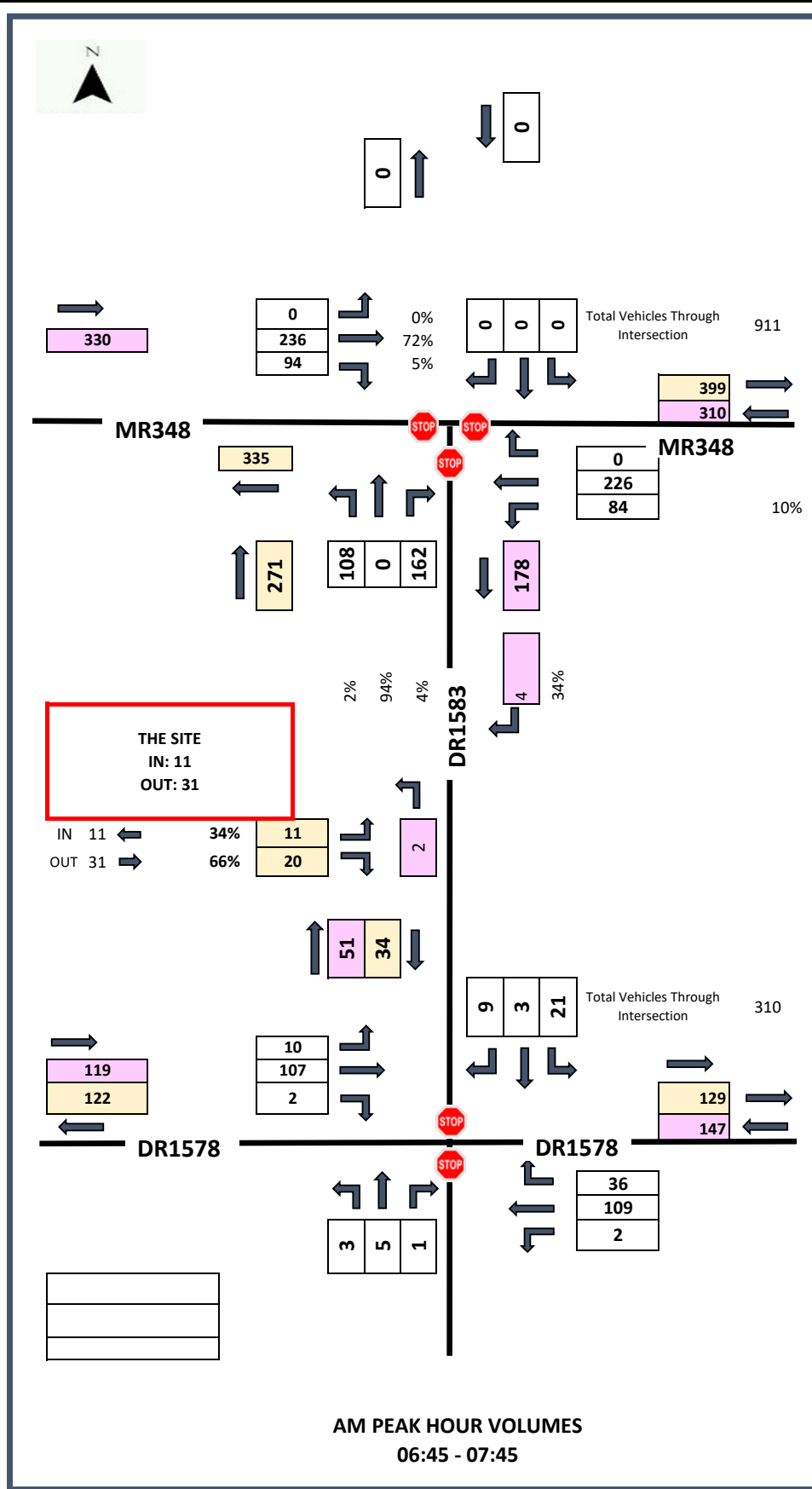


Project:  
**23-041 REM ERF 2833, GREAT BRAK RIVER**

Description:  
**DEVELOPMENT TRIP GENERATION AND DISTRIBUTION**

Legend  
 STOP CONTROLLED INTERSECTION

Title  
**FIGURE D**



**NM PERIOD NOT APPLICABLE**



**Project:**  
23-041 REM ERF 2833, GREAT BRAK RIVER

**Description:**  
2028 BACKGROUND + DEVELOPMENT TRAFFIC

**Legend**  
STOP CONTROLLED INTERSECTION

**Title**  
FIGURE E



# **ANNEXURE E**

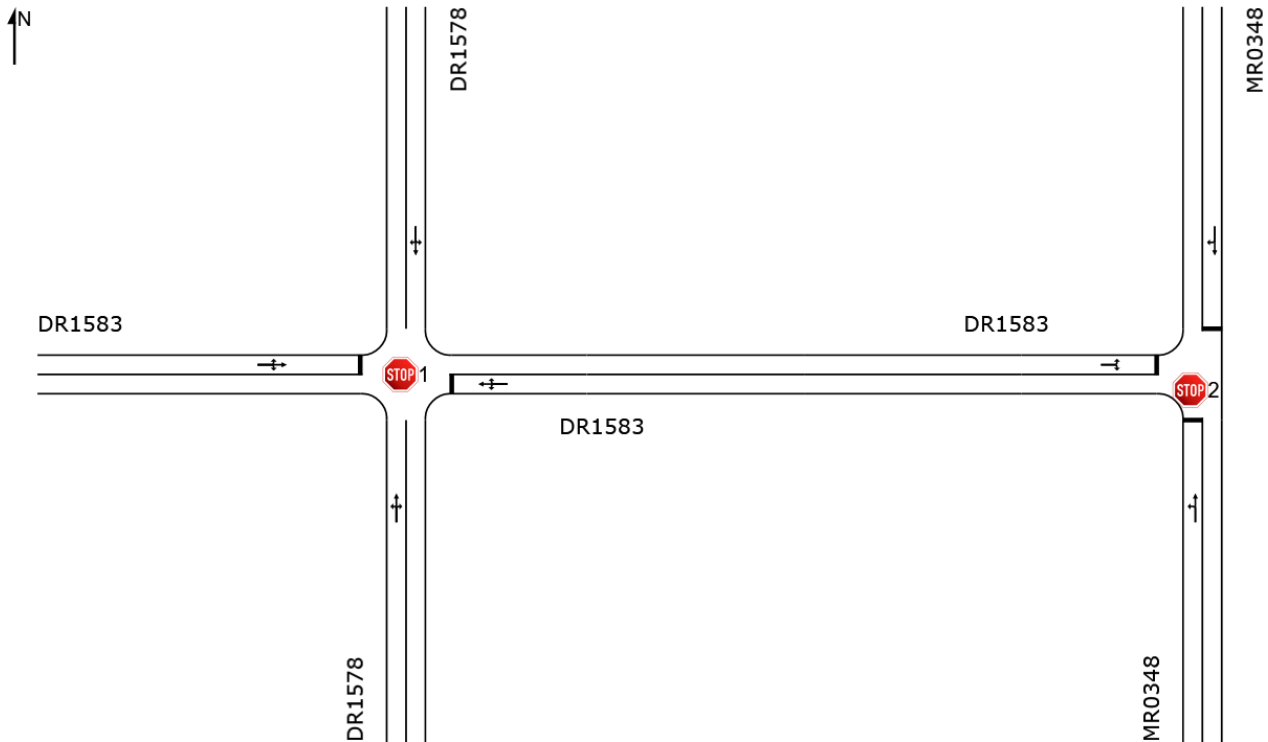
# **SIDRA RESULTS**

# NETWORK LAYOUT

■ Network: N101 [AM Status Quo (Network Folder: Status Quo)]

New Network  
 Network Category: (None)

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.



| SITES IN NETWORK |        |                             |
|------------------|--------|-----------------------------|
| Site ID          | CCG ID | Site Name                   |
| STOP 1           | NA     | DR1578/DR1583 Status Quo AM |
| STOP 2           | NA     | DR1583/MR0348 Satus Quo AM  |

# MOVEMENT SUMMARY

 Site: 1 [DR1578/DR1583 Status Quo AM (Site Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (Two-Way)

| Vehicle Movement Performance |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |      | Arrival Flows |      | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %    | [ Total HV ]  | %    | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |      | veh/h         |      |           |             |                  | veh               | m        |           |                |                     |             |
| South: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 2            | 50,0 | 2             | 50,0 | 0,070     | 6,1         | LOS A            | 0,2               | 1,4      | 0,11      | 0,18           | 0,11                | 53,6        |
| 2                            | T1   | All MCs   | 94           | 6,4  | 94            | 6,4  | 0,070     | 0,0         | LOS A            | 0,2               | 1,4      | 0,11      | 0,18           | 0,11                | 58,2        |
| 3                            | R2   | All MCs   | 30           | 3,3  | 30            | 3,3  | 0,070     | 6,2         | LOS A            | 0,2               | 1,4      | 0,11      | 0,18           | 0,11                | 58,4        |
| Approach                     |      |           | 126          | 6,3  | 126           | 6,3  | 0,070     | 1,6         | NA               | 0,2               | 1,4      | 0,11      | 0,18           | 0,11                | 58,3        |
| East: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 4                            | L2   | All MCs   | 14           | 0,0  | 14            | 0,0  | 0,023     | 8,3         | LOS A            | 0,1               | 0,6      | 0,23      | 0,88           | 0,23                | 56,7        |
| 5                            | T1   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,023     | 8,7         | LOS A            | 0,1               | 0,6      | 0,23      | 0,88           | 0,23                | 56,7        |
| 6                            | R2   | All MCs   | 7            | 0,0  | 7             | 0,0  | 0,023     | 8,8         | LOS A            | 0,1               | 0,6      | 0,23      | 0,88           | 0,23                | 56,6        |
| Approach                     |      |           | 24           | 0,0  | 24            | 0,0  | 0,023     | 8,5         | LOS A            | 0,1               | 0,6      | 0,23      | 0,88           | 0,23                | 56,7        |
| North: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 7                            | L2   | All MCs   | 8            | 0,0  | 8             | 0,0  | 0,053     | 5,5         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,0        |
| 8                            | T1   | All MCs   | 92           | 0,0  | 92            | 0,0  | 0,053     | 0,0         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,4        |
| 9                            | R2   | All MCs   | 2            | 0,0  | 2             | 0,0  | 0,053     | 5,7         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 56,6        |
| Approach                     |      |           | 102          | 0,0  | 102           | 0,0  | 0,053     | 0,5         | NA               | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,3        |
| West: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,008     | 8,3         | LOS A            | 0,0               | 0,2      | 0,26      | 0,89           | 0,26                | 51,0        |
| 11                           | T1   | All MCs   | 4            | 0,0  | 4             | 0,0  | 0,008     | 8,7         | LOS A            | 0,0               | 0,2      | 0,26      | 0,89           | 0,26                | 56,7        |
| 12                           | R2   | All MCs   | 1            | 0,0  | 1             | 0,0  | 0,008     | 8,8         | LOS A            | 0,0               | 0,2      | 0,26      | 0,89           | 0,26                | 50,8        |
| Approach                     |      |           | 8            | 0,0  | 8             | 0,0  | 0,008     | 8,6         | LOS A            | 0,0               | 0,2      | 0,26      | 0,89           | 0,26                | 55,2        |
| All Vehicles                 |      |           | 260          | 3,1  | 260           | 3,1  | 0,070     | 2,0         | NA               | 0,2               | 1,4      | 0,09      | 0,22           | 0,09                | 58,1        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Minor Road Approach LOS values are based on average delay for all vehicle movements.  
 NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).  
 Two-Way Sign Control Capacity Model: SIDRA Standard.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 1 [DR1578/DR1583 Status Quo PM (Site Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (Two-Way)

| Vehicle Movement Performance |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |      | Arrival Flows |      | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %    | [ Total HV ]  | %    | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |      | veh/h         |      |           |             |                  | veh               | m        |           |                |                     |             |
| South: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 22           | 0,0  | 22            | 0,0  | 0,081     | 5,5         | LOS A            | 0,2               | 1,4      | 0,11      | 0,22           | 0,11                | 55,4        |
| 2                            | T1   | All MCs   | 98           | 9,2  | 98            | 9,2  | 0,081     | 0,0         | LOS A            | 0,2               | 1,4      | 0,11      | 0,22           | 0,11                | 57,7        |
| 3                            | R2   | All MCs   | 26           | 0,0  | 26            | 0,0  | 0,081     | 6,4         | LOS A            | 0,2               | 1,4      | 0,11      | 0,22           | 0,11                | 58,3        |
| Approach                     |      |           | 146          | 6,2  | 146           | 6,2  | 0,081     | 2,0         | NA               | 0,2               | 1,4      | 0,11      | 0,22           | 0,11                | 57,7        |
| East: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 4                            | L2   | All MCs   | 22           | 0,0  | 22            | 0,0  | 0,029     | 8,4         | LOS A            | 0,1               | 0,8      | 0,24      | 0,88           | 0,24                | 56,7        |
| 5                            | T1   | All MCs   | 4            | 0,0  | 4             | 0,0  | 0,029     | 9,0         | LOS A            | 0,1               | 0,8      | 0,24      | 0,88           | 0,24                | 56,7        |
| 6                            | R2   | All MCs   | 6            | 0,0  | 6             | 0,0  | 0,029     | 9,0         | LOS A            | 0,1               | 0,8      | 0,24      | 0,88           | 0,24                | 56,6        |
| Approach                     |      |           | 32           | 0,0  | 32            | 0,0  | 0,029     | 8,6         | LOS A            | 0,1               | 0,8      | 0,24      | 0,88           | 0,24                | 56,7        |
| North: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 7                            | L2   | All MCs   | 9            | 0,0  | 9             | 0,0  | 0,063     | 5,5         | LOS A            | 0,0               | 0,3      | 0,02      | 0,07           | 0,02                | 58,9        |
| 8                            | T1   | All MCs   | 102          | 8,8  | 102           | 8,8  | 0,063     | 0,0         | LOS A            | 0,0               | 0,3      | 0,02      | 0,07           | 0,02                | 59,2        |
| 9                            | R2   | All MCs   | 4            | 0,0  | 4             | 0,0  | 0,063     | 6,0         | LOS A            | 0,0               | 0,3      | 0,02      | 0,07           | 0,02                | 56,5        |
| Approach                     |      |           | 115          | 7,8  | 115           | 7,8  | 0,063     | 0,6         | NA               | 0,0               | 0,3      | 0,02      | 0,07           | 0,02                | 59,1        |
| West: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 8            | 12,5 | 8             | 12,5 | 0,089     | 9,0         | LOS A            | 0,3               | 2,2      | 0,35      | 0,89           | 0,35                | 50,2        |
| 11                           | T1   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,089     | 9,0         | LOS A            | 0,3               | 2,2      | 0,35      | 0,89           | 0,35                | 56,6        |
| 12                           | R2   | All MCs   | 60           | 0,0  | 60            | 0,0  | 0,089     | 9,2         | LOS A            | 0,3               | 2,2      | 0,35      | 0,89           | 0,35                | 50,5        |
| Approach                     |      |           | 71           | 1,4  | 71            | 1,4  | 0,089     | 9,2         | LOS A            | 0,3               | 2,2      | 0,35      | 0,89           | 0,35                | 51,1        |
| All Vehicles                 |      |           | 364          | 5,2  | 364           | 5,2  | 0,089     | 3,5         | NA               | 0,3               | 2,2      | 0,14      | 0,36           | 0,14                | 56,7        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Minor Road Approach LOS values are based on average delay for all vehicle movements.  
 NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).  
 Two-Way Sign Control Capacity Model: SIDRA Standard.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 Satus Quo AM (Site Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (All-Way)

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |     | veh/h         |     |           |             |                  | veh               | m        |           |                |                     |             |
| South: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 68           | 2,9 | 68            | 2,9 | 0,468     | 18,1        | LOS C            | 2,1               | 15,3     | 0,89      | 1,35           | 2,74                | 54,5        |
| 2                            | T1   | All MCs   | 195          | 2,1 | 195           | 2,1 | 0,468     | 17,7        | LOS C            | 2,1               | 15,3     | 0,89      | 1,35           | 2,74                | 46,0        |
| Approach                     |      |           | 263          | 2,3 | 263           | 2,3 | 0,468     | 17,8        | LOS C            | 2,1               | 15,3     | 0,89      | 1,35           | 2,74                | 50,0        |
| North: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 8                            | T1   | All MCs   | 204          | 1,5 | 204           | 1,5 | 0,399     | 14,2        | LOS B            | 1,6               | 11,5     | 0,79      | 1,32           | 2,44                | 48,1        |
| 9                            | R2   | All MCs   | 78           | 0,0 | 78            | 0,0 | 0,399     | 13,9        | LOS B            | 1,6               | 11,5     | 0,79      | 1,32           | 2,44                | 55,4        |
| Approach                     |      |           | 282          | 1,1 | 282           | 1,1 | 0,399     | 14,1        | LOS B            | 1,6               | 11,5     | 0,79      | 1,32           | 2,44                | 51,7        |
| West: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 85           | 2,4 | 85            | 2,4 | 0,449     | 19,9        | LOS C            | 2,0               | 14,4     | 0,92      | 1,32           | 2,71                | 54,0        |
| 12                           | R2   | All MCs   | 127          | 0,0 | 127           | 0,0 | 0,449     | 19,2        | LOS C            | 2,0               | 14,4     | 0,92      | 1,32           | 2,71                | 53,9        |
| Approach                     |      |           | 212          | 0,9 | 212           | 0,9 | 0,449     | 19,5        | LOS C            | 2,0               | 14,4     | 0,92      | 1,32           | 2,71                | 54,0        |
| All Vehicles                 |      |           | 757          | 1,5 | 757           | 1,5 | 0,468     | 16,9        | LOS C            | 2,1               | 15,3     | 0,86      | 1,33           | 2,62                | 52,2        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Intersection and Approach LOS values are based on average delay for all vehicle movements.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 Satus Quo PM (Site Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (All-Way)

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |     | veh/h         |     |           |             |                  | veh               | m        |           |                |                     |             |
| South: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 104          | 1,0 | 104           | 1,0 | 0,471     | 16,2        | LOS C            | 2,1               | 15,1     | 0,84      | 1,36           | 2,71                | 55,0        |
| 2                            | T1   | All MCs   | 209          | 1,9 | 209           | 1,9 | 0,471     | 15,9        | LOS C            | 2,1               | 15,1     | 0,84      | 1,36           | 2,71                | 55,0        |
| Approach                     |      |           | 313          | 1,6 | 313           | 1,6 | 0,471     | 16,0        | LOS C            | 2,1               | 15,1     | 0,84      | 1,36           | 2,71                | 55,0        |
| North: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 8                            | T1   | All MCs   | 197          | 0,0 | 197           | 0,0 | 0,345     | 12,4        | LOS B            | 1,3               | 9,1      | 0,72      | 1,30           | 2,23                | 55,9        |
| 9                            | R2   | All MCs   | 81           | 3,7 | 81            | 3,7 | 0,345     | 12,5        | LOS B            | 1,3               | 9,1      | 0,72      | 1,30           | 2,23                | 48,7        |
| Approach                     |      |           | 278          | 1,1 | 278           | 1,1 | 0,345     | 12,4        | LOS B            | 1,3               | 9,1      | 0,72      | 1,30           | 2,23                | 54,9        |
| West: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 79           | 1,3 | 79            | 1,3 | 0,387     | 19,8        | LOS C            | 1,6               | 11,6     | 0,92      | 1,28           | 2,53                | 45,0        |
| 12                           | R2   | All MCs   | 86           | 1,2 | 86            | 1,2 | 0,387     | 19,2        | LOS C            | 1,6               | 11,6     | 0,92      | 1,28           | 2,53                | 53,9        |
| Approach                     |      |           | 165          | 1,2 | 165           | 1,2 | 0,387     | 19,5        | LOS C            | 1,6               | 11,6     | 0,92      | 1,28           | 2,53                | 51,5        |
| All Vehicles                 |      |           | 756          | 1,3 | 756           | 1,3 | 0,471     | 15,5        | LOS C            | 2,1               | 15,1     | 0,81      | 1,32           | 2,50                | 54,3        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Intersection and Approach LOS values are based on average delay for all vehicle movements.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# LEVEL OF SERVICE

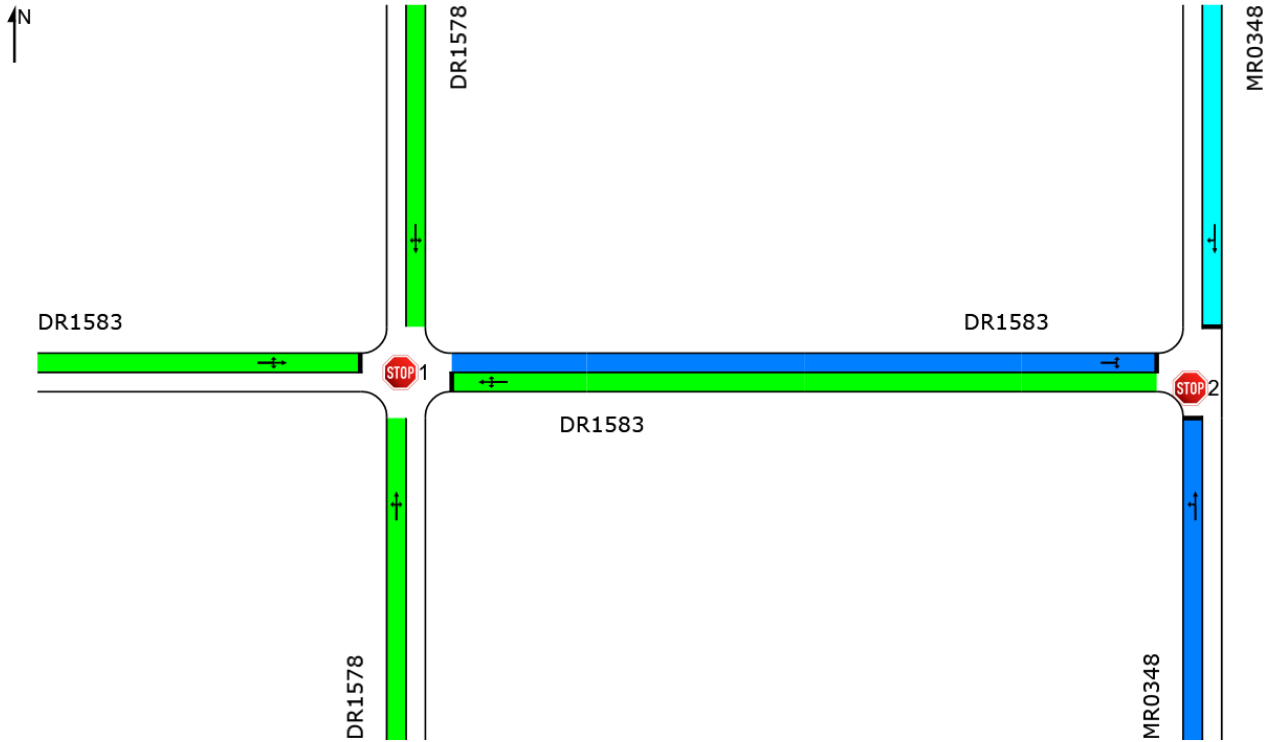
Lane Level of Service

■ Network: N101 [AM Status Quo (Network Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)



Colour code based on Level of Service



Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

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# MOVEMENT SUMMARY

**Site: 1 [DR1578/DR1583 2028 AM (Site Folder: Future 2028)]**

**Output produced by SIDRA INTERSECTION Version: 9.1.3.210**

New Site

Site Category: (None)

Stop (Two-Way)

Design Life Analysis: Constant Number of Years = 5

| Vehicle Movement Performance |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|--------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |      | Arrival Flows |      | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |        | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %    | [ Total HV ]  | %    | v/c       | sec         |                  | [ Veh. veh        | Dist ] |           |                |                     | km/h        |
|                              |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
| South: DR1578                |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
| 1                            | L2   | All MCs   | 2            | 50,0 | 2             | 50,0 | 0,091     | 6,1         | LOSA             | 0,2               | 1,8    | 0,13      | 0,19           | 0,13                | 53,5        |
| 2                            | T1   | All MCs   | 120          | 6,4  | 120           | 6,4  | 0,091     | 0,0         | LOSA             | 0,2               | 1,8    | 0,13      | 0,19           | 0,13                | 58,1        |
| 3                            | R2   | All MCs   | 39           | 3,3  | 39            | 3,3  | 0,091     | 6,4         | LOSA             | 0,2               | 1,8    | 0,13      | 0,19           | 0,13                | 58,4        |
| Approach                     |      |           | 161          | 6,2  | 161           | 6,2  | 0,091     | 1,6         | NA               | 0,2               | 1,8    | 0,13      | 0,19           | 0,13                | 58,2        |
| East: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
| 4                            | L2   | All MCs   | 18           | 0,0  | 18            | 0,0  | 0,030     | 8,4         | LOSA             | 0,1               | 0,7    | 0,27      | 0,87           | 0,27                | 56,7        |
| 5                            | T1   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,030     | 9,1         | LOSA             | 0,1               | 0,7    | 0,27      | 0,87           | 0,27                | 56,7        |
| 6                            | R2   | All MCs   | 9            | 0,0  | 9             | 0,0  | 0,030     | 9,3         | LOSA             | 0,1               | 0,7    | 0,27      | 0,87           | 0,27                | 56,6        |
| Approach                     |      |           | 30           | 0,0  | 30            | 0,0  | 0,030     | 8,8         | LOSA             | 0,1               | 0,7    | 0,27      | 0,87           | 0,27                | 56,6        |
| North: DR1578                |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
| 7                            | L2   | All MCs   | 10           | 0,0  | 10            | 0,0  | 0,067     | 5,5         | LOSA             | 0,0               | 0,1    | 0,01      | 0,06           | 0,01                | 59,0        |
| 8                            | T1   | All MCs   | 118          | 0,0  | 118           | 0,0  | 0,067     | 0,0         | LOSA             | 0,0               | 0,1    | 0,01      | 0,06           | 0,01                | 59,4        |
| 9                            | R2   | All MCs   | 2            | 0,0  | 2             | 0,0  | 0,067     | 5,8         | LOSA             | 0,0               | 0,1    | 0,01      | 0,06           | 0,01                | 56,7        |
| Approach                     |      |           | 130          | 0,0  | 130           | 0,0  | 0,067     | 0,5         | NA               | 0,0               | 0,1    | 0,01      | 0,06           | 0,01                | 59,3        |
| West: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |        |           |                |                     |             |
| 10                           | L2   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,010     | 8,4         | LOSA             | 0,0               | 0,3    | 0,31      | 0,88           | 0,31                | 50,9        |
| 11                           | T1   | All MCs   | 6            | 0,0  | 6             | 0,0  | 0,010     | 9,1         | LOSA             | 0,0               | 0,3    | 0,31      | 0,88           | 0,31                | 56,7        |
| 12                           | R2   | All MCs   | 1            | 0,0  | 1             | 0,0  | 0,010     | 9,3         | LOSA             | 0,0               | 0,3    | 0,31      | 0,88           | 0,31                | 50,7        |
| Approach                     |      |           | 10           | 0,0  | 10            | 0,0  | 0,010     | 8,9         | LOSA             | 0,0               | 0,3    | 0,31      | 0,88           | 0,31                | 55,3        |
| All Vehicles                 |      |           | 331          | 3,0  | 331           | 3,0  | 0,091     | 2,0         | NA               | 0,2               | 1,8    | 0,10      | 0,22           | 0,10                | 58,1        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).

Two-Way Sign Control Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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# MOVEMENT SUMMARY

 Site: 1 [DR1578/DR1583 2028 PM (Site Folder: Future 2028)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site

Site Category: (None)

Stop (Two-Way)

| Vehicle Movement Performance |      |           |                       |      |                       |      |           |             |                  |                   |               |           |                |                     |             |
|------------------------------|------|-----------|-----------------------|------|-----------------------|------|-----------|-------------|------------------|-------------------|---------------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows          |      | Arrival Flows         |      | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |               | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ]<br>veh/h | %    | [ Total HV ]<br>veh/h | %    |           |             |                  | [ Veh. ]<br>veh   | [ Dist ]<br>m |           |                |                     |             |
| South: DR1578                |      |           |                       |      |                       |      |           |             |                  |                   |               |           |                |                     |             |
| 1                            | L2   | All MCs   | 26                    | 0,0  | 26                    | 0,0  | 0,095     | 5,5         | LOS A            | 0,2               | 1,7           | 0,12      | 0,22           | 0,12                | 55,4        |
| 2                            | T1   | All MCs   | 114                   | 9,2  | 114                   | 9,2  | 0,095     | 0,0         | LOS A            | 0,2               | 1,7           | 0,12      | 0,22           | 0,12                | 57,7        |
| 3                            | R2   | All MCs   | 30                    | 0,0  | 30                    | 0,0  | 0,095     | 6,5         | LOS A            | 0,2               | 1,7           | 0,12      | 0,22           | 0,12                | 58,3        |
| Approach                     |      |           | 170                   | 6,2  | 170                   | 6,2  | 0,095     | 2,0         | NA               | 0,2               | 1,7           | 0,12      | 0,22           | 0,12                | 57,7        |
| East: DR1583                 |      |           |                       |      |                       |      |           |             |                  |                   |               |           |                |                     |             |
| 4                            | L2   | All MCs   | 26                    | 0,0  | 26                    | 0,0  | 0,036     | 8,5         | LOS A            | 0,1               | 0,9           | 0,27      | 0,87           | 0,27                | 56,7        |
| 5                            | T1   | All MCs   | 5                     | 0,0  | 5                     | 0,0  | 0,036     | 9,2         | LOS A            | 0,1               | 0,9           | 0,27      | 0,87           | 0,27                | 56,7        |
| 6                            | R2   | All MCs   | 7                     | 0,0  | 7                     | 0,0  | 0,036     | 9,3         | LOS A            | 0,1               | 0,9           | 0,27      | 0,87           | 0,27                | 56,6        |
| Approach                     |      |           | 38                    | 0,0  | 38                    | 0,0  | 0,036     | 8,7         | LOS A            | 0,1               | 0,9           | 0,27      | 0,87           | 0,27                | 56,6        |
| North: DR1578                |      |           |                       |      |                       |      |           |             |                  |                   |               |           |                |                     |             |
| 7                            | L2   | All MCs   | 10                    | 0,0  | 10                    | 0,0  | 0,073     | 5,5         | LOS A            | 0,0               | 0,3           | 0,03      | 0,07           | 0,03                | 58,9        |
| 8                            | T1   | All MCs   | 118                   | 8,8  | 118                   | 8,8  | 0,073     | 0,0         | LOS A            | 0,0               | 0,3           | 0,03      | 0,07           | 0,03                | 59,2        |
| 9                            | R2   | All MCs   | 5                     | 0,0  | 5                     | 0,0  | 0,073     | 6,3         | LOS A            | 0,0               | 0,3           | 0,03      | 0,07           | 0,03                | 56,5        |
| Approach                     |      |           | 133                   | 7,8  | 133                   | 7,8  | 0,073     | 0,7         | NA               | 0,0               | 0,3           | 0,03      | 0,07           | 0,03                | 59,1        |
| West: DR1583                 |      |           |                       |      |                       |      |           |             |                  |                   |               |           |                |                     |             |
| 10                           | L2   | All MCs   | 9                     | 12,5 | 9                     | 12,5 | 0,109     | 9,1         | LOS A            | 0,4               | 2,7           | 0,39      | 0,90           | 0,39                | 50,0        |
| 11                           | T1   | All MCs   | 3                     | 0,0  | 3                     | 0,0  | 0,109     | 9,3         | LOS A            | 0,4               | 2,7           | 0,39      | 0,90           | 0,39                | 56,5        |
| 12                           | R2   | All MCs   | 70                    | 0,0  | 70                    | 0,0  | 0,109     | 9,6         | LOS A            | 0,4               | 2,7           | 0,39      | 0,90           | 0,39                | 50,2        |
| Approach                     |      |           | 82                    | 1,4  | 82                    | 1,4  | 0,109     | 9,6         | LOS A            | 0,4               | 2,7           | 0,39      | 0,90           | 0,39                | 50,8        |
| All Vehicles                 |      |           | 423                   | 5,2  | 423                   | 5,2  | 0,109     | 3,6         | NA               | 0,4               | 2,7           | 0,15      | 0,37           | 0,15                | 56,7        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).

Two-Way Sign Control Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 2028 AM (Site Folder: Future 2028)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site

Site Category: (None)

Stop (All-Way)

| Vehicle Movement Performance |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
|------------------------------|------|-----------|-----------------------|-----|-----------------------|-----|-----------|-------------|------------------|-------------------|---------------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows          |     | Arrival Flows         |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |               | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ]<br>veh/h | %   | [ Total HV ]<br>veh/h | %   |           |             |                  | [ Veh. ]<br>veh   | [ Dist ]<br>m |           |                |                     |             |
| South: MR0348                |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 1                            | L2   | All MCs   | 79                    | 2,9 | 79                    | 2,9 | 0,542     | 20,0        | LOS C            | 2,8               | 19,7          | 0,91      | 1,42           | 3,06                | 54,0        |
| 2                            | T1   | All MCs   | 226                   | 2,1 | 226                   | 2,1 | 0,542     | 19,6        | LOS C            | 2,8               | 19,7          | 0,91      | 1,42           | 3,06                | 45,0        |
| Approach                     |      |           | 305                   | 2,3 | 305                   | 2,3 | 0,542     | 19,7        | LOS C            | 2,8               | 19,7          | 0,91      | 1,42           | 3,06                | 49,2        |
| North: MR0348                |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 8                            | T1   | All MCs   | 236                   | 1,5 | 236                   | 1,5 | 0,461     | 15,2        | LOS C            | 2,0               | 14,5          | 0,82      | 1,36           | 2,65                | 47,5        |
| 9                            | R2   | All MCs   | 90                    | 0,0 | 90                    | 0,0 | 0,461     | 14,8        | LOS B            | 2,0               | 14,5          | 0,82      | 1,36           | 2,65                | 55,1        |
| Approach                     |      |           | 326                   | 1,1 | 326                   | 1,1 | 0,461     | 15,1        | LOS C            | 2,0               | 14,5          | 0,82      | 1,36           | 2,65                | 51,3        |
| West: DR1583                 |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 10                           | L2   | All MCs   | 99                    | 2,4 | 99                    | 2,4 | 0,520     | 21,9        | LOS C            | 2,6               | 18,3          | 0,94      | 1,38           | 2,99                | 53,5        |
| 12                           | R2   | All MCs   | 147                   | 0,0 | 147                   | 0,0 | 0,520     | 21,1        | LOS C            | 2,6               | 18,3          | 0,94      | 1,38           | 2,99                | 53,4        |
| Approach                     |      |           | 246                   | 0,9 | 246                   | 0,9 | 0,520     | 21,4        | LOS C            | 2,6               | 18,3          | 0,94      | 1,38           | 2,99                | 53,5        |
| All Vehicles                 |      |           | 877                   | 1,5 | 877                   | 1,5 | 0,542     | 18,5        | LOS C            | 2,8               | 19,7          | 0,88      | 1,38           | 2,89                | 51,6        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 2028 PM (Site Folder: Future 2028)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site

Site Category: (None)

Stop (All-Way)

| Vehicle Movement Performance |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
|------------------------------|------|-----------|-----------------------|-----|-----------------------|-----|-----------|-------------|------------------|-------------------|---------------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows          |     | Arrival Flows         |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |               | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ]<br>veh/h | %   | [ Total HV ]<br>veh/h | %   |           |             |                  | [ Veh. ]<br>veh   | [ Dist ]<br>m |           |                |                     |             |
| South: MR0348                |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 1                            | L2   | All MCs   | 121                   | 1,0 | 121                   | 1,0 | 0,543     | 17,7        | LOS C            | 2,7               | 19,5          | 0,87      | 1,42           | 3,02                | 54,6        |
| 2                            | T1   | All MCs   | 242                   | 1,9 | 242                   | 1,9 | 0,543     | 17,5        | LOS C            | 2,7               | 19,5          | 0,87      | 1,42           | 3,02                | 46,1        |
| Approach                     |      |           | 363                   | 1,6 | 363                   | 1,6 | 0,543     | 17,6        | LOS C            | 2,7               | 19,5          | 0,87      | 1,42           | 3,02                | 50,9        |
| North: MR0348                |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 8                            | T1   | All MCs   | 232                   | 0,0 | 232                   | 0,0 | 0,399     | 13,1        | LOS B            | 1,6               | 11,3          | 0,74      | 1,33           | 2,39                | 48,7        |
| 9                            | R2   | All MCs   | 90                    | 3,7 | 90                    | 3,7 | 0,399     | 13,1        | LOS B            | 1,6               | 11,3          | 0,74      | 1,33           | 2,39                | 55,6        |
| Approach                     |      |           | 322                   | 1,0 | 322                   | 1,0 | 0,399     | 13,1        | LOS B            | 1,6               | 11,3          | 0,74      | 1,33           | 2,39                | 52,2        |
| West: DR1583                 |      |           |                       |     |                       |     |           |             |                  |                   |               |           |                |                     |             |
| 10                           | L2   | All MCs   | 92                    | 1,3 | 92                    | 1,3 | 0,447     | 21,1        | LOS C            | 2,0               | 14,4          | 0,94      | 1,32           | 2,72                | 53,7        |
| 12                           | R2   | All MCs   | 100                   | 1,2 | 100                   | 1,2 | 0,447     | 20,6        | LOS C            | 2,0               | 14,4          | 0,94      | 1,32           | 2,72                | 53,6        |
| Approach                     |      |           | 192                   | 1,2 | 192                   | 1,2 | 0,447     | 20,8        | LOS C            | 2,0               | 14,4          | 0,94      | 1,32           | 2,72                | 53,6        |
| All Vehicles                 |      |           | 877                   | 1,3 | 877                   | 1,3 | 0,543     | 16,6        | LOS C            | 2,7               | 19,5          | 0,84      | 1,37           | 2,73                | 52,2        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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# NETWORK SUMMARY

■ ■ Network: N101 [AM Status Quo (Network Folder: Status Quo)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)

| Network Performance - Hourly Values  |           |         |                  |
|--------------------------------------|-----------|---------|------------------|
| Performance Measure                  | Vehicles: | All MCs | Persons          |
| Network Level of Service (LOS)       |           | LOS B   |                  |
| Speed Efficiency                     |           | 0,86    |                  |
| Travel Time Index                    |           | 8,46    |                  |
| Congestion Coefficient               |           | 1,16    |                  |
| Travel Speed (Average)               | km/h      | 51,7    | 51,7 km/h        |
| Travel Distance (Total)              | veh-km/h  | 1418,1  | 1701,7 pers-km/h |
| Travel Time (Total)                  | veh-h/h   | 27,4    | 32,9 pers-h/h    |
| Desired Speed                        | km/h      | 60,0    |                  |
| Demand Flows (Total for all Sites)   | veh/h     | 1017    | 1220 pers/h      |
| Arrival Flows (Total for all Sites)  | veh/h     | 1017    | 1220 pers/h      |
| Demand Flows (Entry Total)           | veh/h     | 781     |                  |
| Midblock Inflows (Total)             | veh/h     | 170     |                  |
| Midblock Outflows (Total)            | veh/h     | -122    |                  |
| Percent Heavy Vehicles (Demand)      | %         | 1,9     |                  |
| Percent Heavy Vehicles (Arrival)     | %         | 1,9     |                  |
| Degree of Saturation                 |           | 0,468   |                  |
| Control Delay (Total)                | veh-h/h   | 3,70    | 4,44 pers-h/h    |
| Control Delay (Average)              | sec       | 13,1    | 13,1 sec         |
| Control Delay (Worst Lane by MC)     | sec       | 19,5    |                  |
| Control Delay (Worst Movement by MC) | sec       | 23,6    | 23,6 sec         |
| Geometric Delay (Average)            | sec       | 6,2     |                  |
| Stop-Line Delay (Average)            | sec       | 6,9     |                  |
| Ave. Que Storage Ratio (Worst Lane)  |           | 0,02    |                  |
| Effective Stops (Total)              | veh/h     | 1065    | 1278 pers/h      |
| Effective Stop Rate                  |           | 1,05    | 1,05             |
| Proportion Queued                    |           | 0,66    | 0,66             |
| Performance Index                    |           | 45,6    | 45,6             |
| Cost (Total) *                       | \$/h      | 1252,64 | 1252,64 \$/h     |
| Fuel Consumption (Total)             | L/h       | 112,8   |                  |
| Fuel Economy                         | L/100km   | 8,0     |                  |
| Carbon Dioxide (Total)               | kg/h      | 266,0   |                  |
| Hydrocarbons (Total)                 | kg/h      | 0,022   |                  |
| Carbon Monoxide (Total)              | kg/h      | 0,31    |                  |
| NOx (Total)                          | kg/h      | 0,241   |                  |

Network Model Variability Index (Average value of largest changes in Lane Degrees of Saturation or Queue Storage Ratios from the third to the last Network Iterations): 0,0 %

Number of Iterations: 5 (Maximum: 30)

Largest change in Lane Degrees of Saturation or Queue Storage Ratios for the last three Network Iterations: 0,0% 0,0% 0,0%

Network Level of Service (LOS) Method: SIDRA Speed Efficiency.

Software Setup used: Standard Left.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

| Network Performance - Annual Values |           |         |                   |
|-------------------------------------|-----------|---------|-------------------|
| Performance Measure                 | Vehicles: | All MCs | Persons           |
| Demand Flows (Total for all Sites)  | veh/y     | 488 160 | 585 792 pers/y    |
| Delay (Total)                       | veh-h/y   | 1 776   | 2 131 pers-h/y    |
| Effective Stops (Total)             | veh/y     | 511 203 | 613 443 pers/y    |
| Travel Distance (Total)             | veh-km/y  | 680 675 | 816 811 pers-km/y |
| Travel Time (Total)                 | veh-h/y   | 13 169  | 15 803 pers-h/y   |
| Cost (Total)                        | \$/y      | 601 265 | 601 265 \$/y      |

|                          |      |         |
|--------------------------|------|---------|
| Fuel Consumption (Total) | L/y  | 54 121  |
| Carbon Dioxide (Total)   | kg/y | 127 681 |
| Hydrocarbons (Total)     | kg/y | 10      |
| Carbon Monoxide (Total)  | kg/y | 151     |
| NOx (Total)              | kg/y | 115     |

1 Hours per Year: 480 (Network)

# LEVEL OF SERVICE

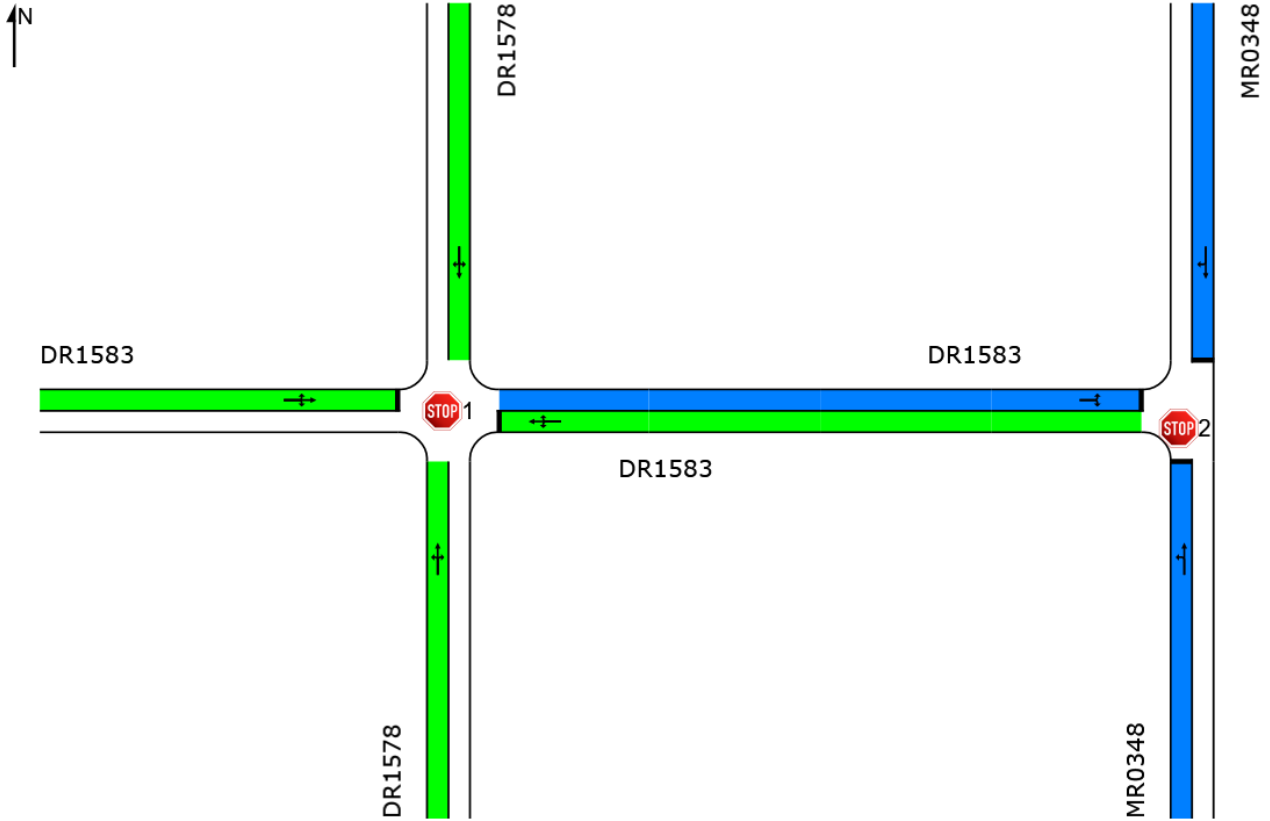
Lane Level of Service

■ Network: N101 [2028 AM (Network Folder: 2028)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)



Colour code based on Level of Service



Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

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# MOVEMENT SUMMARY

 Site: 1 [DR1578/DR1583 2028 + Dev AM (Site Folder: Future 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (Two-Way)  
 Design Life Analysis: Constant Number of Years = 5

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   |           |             |                  | [ Veh. ]          | [ Dist ] |           |                |                     |             |
|                              |      |           | veh/h        | %   | veh/h         | %   | v/c       | sec         |                  | veh               | m        |           |                |                     | km/h        |
| South: DR1578                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 250          | 0   | 250           | 0   | 0,092     | 6,1         | LOS A            | 0,3               | 1,9      | 0,13      | 0,19           | 0,13                | 53,5        |
| 2                            | T1   | All MCs   | 120          | 6,4 | 120           | 6,4 | 0,092     | 0,0         | LOS A            | 0,3               | 1,9      | 0,13      | 0,19           | 0,13                | 58,1        |
| 3                            | R2   | All MCs   | 40           | 3,3 | 40            | 3,3 | 0,092     | 6,4         | LOS A            | 0,3               | 1,9      | 0,13      | 0,19           | 0,13                | 58,4        |
| Approach                     |      |           | 162          | 6,2 | 162           | 6,2 | 0,092     | 1,6         | NA               | 0,3               | 1,9      | 0,13      | 0,19           | 0,13                | 58,2        |
| East: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 4                            | L2   | All MCs   | 23           | 0,0 | 23            | 0,0 | 0,035     | 8,4         | LOS A            | 0,1               | 0,9      | 0,27      | 0,87           | 0,27                | 56,7        |
| 5                            | T1   | All MCs   | 3            | 0,0 | 3             | 0,0 | 0,035     | 9,1         | LOS A            | 0,1               | 0,9      | 0,27      | 0,87           | 0,27                | 56,7        |
| 6                            | R2   | All MCs   | 10           | 0,0 | 10            | 0,0 | 0,035     | 9,3         | LOS A            | 0,1               | 0,9      | 0,27      | 0,87           | 0,27                | 56,6        |
| Approach                     |      |           | 36           | 0,0 | 36            | 0,0 | 0,035     | 8,7         | LOS A            | 0,1               | 0,9      | 0,27      | 0,87           | 0,27                | 56,6        |
| North: DR1578                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 7                            | L2   | All MCs   | 11           | 0,0 | 11            | 0,0 | 0,068     | 5,5         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,0        |
| 8                            | T1   | All MCs   | 118          | 0,0 | 118           | 0,0 | 0,068     | 0,0         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,4        |
| 9                            | R2   | All MCs   | 2            | 0,0 | 2             | 0,0 | 0,068     | 5,8         | LOS A            | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 56,6        |
| Approach                     |      |           | 131          | 0,0 | 131           | 0,0 | 0,068     | 0,6         | NA               | 0,0               | 0,1      | 0,01      | 0,06           | 0,01                | 59,3        |
| West: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 3            | 0,0 | 3             | 0,0 | 0,010     | 8,4         | LOS A            | 0,0               | 0,3      | 0,31      | 0,88           | 0,31                | 50,9        |
| 11                           | T1   | All MCs   | 6            | 0,0 | 6             | 0,0 | 0,010     | 9,1         | LOS A            | 0,0               | 0,3      | 0,31      | 0,88           | 0,31                | 56,6        |
| 12                           | R2   | All MCs   | 1            | 0,0 | 1             | 0,0 | 0,010     | 9,3         | LOS A            | 0,0               | 0,3      | 0,31      | 0,88           | 0,31                | 50,6        |
| Approach                     |      |           | 10           | 0,0 | 10            | 0,0 | 0,010     | 8,9         | LOS A            | 0,0               | 0,3      | 0,31      | 0,88           | 0,31                | 55,3        |
| All Vehicles                 |      |           | 340          | 3,0 | 340           | 3,0 | 0,092     | 2,2         | NA               | 0,3               | 1,9      | 0,11      | 0,23           | 0,11                | 58,0        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Minor Road Approach LOS values are based on average delay for all vehicle movements.  
 NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).  
 Two-Way Sign Control Capacity Model: SIDRA Standard.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 1 [DR1578/DR1583 2028 + Dev PM (Site Folder: Future 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
Site Category: (None)  
Stop (Two-Way)

| Vehicle Movement Performance |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|------|---------------|------|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |      | Arrival Flows |      | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %    | [ Total HV ]  | %    | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |      | veh/h         |      |           |             |                  | veh               | m        |           |                |                     |             |
| South: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 26           | 0,0  | 26            | 0,0  | 0,098     | 5,5         | LOS A            | 0,3               | 1,9      | 0,13      | 0,24           | 0,13                | 55,3        |
| 2                            | T1   | All MCs   | 114          | 9,2  | 114           | 9,2  | 0,098     | 0,0         | LOS A            | 0,3               | 1,9      | 0,13      | 0,24           | 0,13                | 57,6        |
| 3                            | R2   | All MCs   | 35           | 0,0  | 35            | 0,0  | 0,098     | 6,5         | LOS A            | 0,3               | 1,9      | 0,13      | 0,24           | 0,13                | 58,2        |
| Approach                     |      |           | 175          | 6,0  | 175           | 6,0  | 0,098     | 2,1         | NA               | 0,3               | 1,9      | 0,13      | 0,24           | 0,13                | 57,6        |
| East: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 4                            | L2   | All MCs   | 27           | 0,0  | 27            | 0,0  | 0,038     | 8,5         | LOS A            | 0,1               | 1,0      | 0,27      | 0,87           | 0,27                | 56,7        |
| 5                            | T1   | All MCs   | 5            | 0,0  | 5             | 0,0  | 0,038     | 9,3         | LOS A            | 0,1               | 1,0      | 0,27      | 0,87           | 0,27                | 56,7        |
| 6                            | R2   | All MCs   | 8            | 0,0  | 8             | 0,0  | 0,038     | 9,3         | LOS A            | 0,1               | 1,0      | 0,27      | 0,87           | 0,27                | 56,6        |
| Approach                     |      |           | 40           | 0,0  | 40            | 0,0  | 0,038     | 8,7         | LOS A            | 0,1               | 1,0      | 0,27      | 0,87           | 0,27                | 56,6        |
| North: DR1578                |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 7                            | L2   | All MCs   | 12           | 0,0  | 12            | 0,0  | 0,074     | 5,5         | LOS A            | 0,0               | 0,3      | 0,03      | 0,08           | 0,03                | 58,9        |
| 8                            | T1   | All MCs   | 118          | 8,8  | 118           | 8,8  | 0,074     | 0,0         | LOS A            | 0,0               | 0,3      | 0,03      | 0,08           | 0,03                | 59,1        |
| 9                            | R2   | All MCs   | 5            | 0,0  | 5             | 0,0  | 0,074     | 6,3         | LOS A            | 0,0               | 0,3      | 0,03      | 0,08           | 0,03                | 56,4        |
| Approach                     |      |           | 135          | 7,7  | 135           | 7,7  | 0,074     | 0,7         | NA               | 0,0               | 0,3      | 0,03      | 0,08           | 0,03                | 59,0        |
| West: DR1583                 |      |           |              |      |               |      |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 9            | 12,5 | 9             | 12,5 | 0,110     | 9,1         | LOS A            | 0,4               | 2,7      | 0,39      | 0,91           | 0,39                | 50,0        |
| 11                           | T1   | All MCs   | 3            | 0,0  | 3             | 0,0  | 0,110     | 9,4         | LOS A            | 0,4               | 2,7      | 0,39      | 0,91           | 0,39                | 56,5        |
| 12                           | R2   | All MCs   | 70           | 0,0  | 70            | 0,0  | 0,110     | 9,7         | LOS A            | 0,4               | 2,7      | 0,39      | 0,91           | 0,39                | 50,2        |
| Approach                     |      |           | 82           | 1,4  | 82            | 1,4  | 0,110     | 9,6         | LOS A            | 0,4               | 2,7      | 0,39      | 0,91           | 0,39                | 50,8        |
| All Vehicles                 |      |           | 432          | 5,1  | 432           | 5,1  | 0,110     | 3,7         | NA               | 0,4               | 2,7      | 0,16      | 0,37           | 0,16                | 56,7        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).

Vehicle movement LOS values are based on average delay per movement.

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA (TWSC): Level of Service is not defined for major road approaches or the intersection as a whole for Two-Way Sign Control (HCM LOS rule).

Two-Way Sign Control Capacity Model: SIDRA Standard.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

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# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 2028 + Dev AM (Site Folder: Future 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (All-Way)

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |     | veh/h         |     |           |             |                  | veh               | m        |           |                |                     |             |
| South: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 84           | 2,9 | 84            | 2,9 | 0,568     | 21,3        | LOS C            | 3,0               | 21,7     | 0,93      | 1,44           | 3,20                | 53,7        |
| 2                            | T1   | All MCs   | 226          | 2,1 | 226           | 2,1 | 0,568     | 20,9        | LOS C            | 3,0               | 21,7     | 0,93      | 1,44           | 3,20                | 44,3        |
| Approach                     |      |           | 310          | 2,3 | 310           | 2,3 | 0,568     | 21,0        | LOS C            | 3,0               | 21,7     | 0,93      | 1,44           | 3,20                | 48,8        |
| North: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 8                            | T1   | All MCs   | 236          | 1,5 | 236           | 1,5 | 0,476     | 15,6        | LOS C            | 2,2               | 15,3     | 0,83      | 1,37           | 2,72                | 47,3        |
| 9                            | R2   | All MCs   | 94           | 0,0 | 94            | 0,0 | 0,476     | 15,3        | LOS C            | 2,2               | 15,3     | 0,83      | 1,37           | 2,72                | 55,0        |
| Approach                     |      |           | 330          | 1,1 | 330           | 1,1 | 0,476     | 15,5        | LOS C            | 2,2               | 15,3     | 0,83      | 1,37           | 2,72                | 51,2        |
| West: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 108          | 2,4 | 108           | 2,4 | 0,551     | 22,4        | LOS C            | 2,9               | 20,4     | 0,94      | 1,41           | 3,13                | 53,4        |
| 12                           | R2   | All MCs   | 162          | 0,0 | 162           | 0,0 | 0,551     | 21,6        | LOS C            | 2,9               | 20,4     | 0,94      | 1,41           | 3,13                | 53,3        |
| Approach                     |      |           | 270          | 0,9 | 270           | 0,9 | 0,551     | 21,9        | LOS C            | 2,9               | 20,4     | 0,94      | 1,41           | 3,13                | 53,3        |
| All Vehicles                 |      |           | 910          | 1,4 | 910           | 1,4 | 0,568     | 19,3        | LOS C            | 3,0               | 21,7     | 0,90      | 1,41           | 3,00                | 51,5        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Intersection and Approach LOS values are based on average delay for all vehicle movements.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# MOVEMENT SUMMARY

 Site: 2 [DR1583/MR0348 2028 + Dev PM (Site Folder: Future 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Site  
 Site Category: (None)  
 Stop (All-Way)

| Vehicle Movement Performance |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
|------------------------------|------|-----------|--------------|-----|---------------|-----|-----------|-------------|------------------|-------------------|----------|-----------|----------------|---------------------|-------------|
| Mov ID                       | Turn | Mov Class | Demand Flows |     | Arrival Flows |     | Deg. Satn | Aver. Delay | Level of Service | 95% Back Of Queue |          | Prop. Que | Eff. Stop Rate | Aver. No. of Cycles | Aver. Speed |
|                              |      |           | [ Total HV ] | %   | [ Total HV ]  | %   | v/c       | sec         |                  | [ Veh. ]          | [ Dist ] |           |                |                     | km/h        |
|                              |      |           | veh/h        |     | veh/h         |     |           |             |                  | veh               | m        |           |                |                     |             |
| South: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 1                            | L2   | All MCs   | 133          | 1,0 | 133           | 1,0 | 0,568     | 18,6        | LOS C            | 3,0               | 21,3     | 0,88      | 1,45           | 3,16                | 54,4        |
| 2                            | T1   | All MCs   | 242          | 1,9 | 242           | 1,9 | 0,568     | 18,3        | LOS C            | 3,0               | 21,3     | 0,88      | 1,45           | 3,16                | 45,7        |
| Approach                     |      |           | 375          | 1,6 | 375           | 1,6 | 0,568     | 18,4        | LOS C            | 3,0               | 21,3     | 0,88      | 1,45           | 3,16                | 50,7        |
| North: MR0348                |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 8                            | T1   | All MCs   | 232          | 0,0 | 232           | 0,0 | 0,412     | 13,2        | LOS B            | 1,7               | 11,8     | 0,74      | 1,34           | 2,43                | 48,6        |
| 9                            | R2   | All MCs   | 102          | 3,7 | 102           | 3,7 | 0,412     | 13,2        | LOS B            | 1,7               | 11,8     | 0,74      | 1,34           | 2,43                | 55,6        |
| Approach                     |      |           | 334          | 1,1 | 334           | 1,1 | 0,412     | 13,2        | LOS B            | 1,7               | 11,8     | 0,74      | 1,34           | 2,43                | 52,4        |
| West: DR1583                 |      |           |              |     |               |     |           |             |                  |                   |          |           |                |                     |             |
| 10                           | L2   | All MCs   | 96           | 1,3 | 96            | 1,3 | 0,465     | 21,6        | LOS C            | 2,2               | 15,3     | 0,94      | 1,33           | 2,78                | 53,5        |
| 12                           | R2   | All MCs   | 104          | 1,2 | 104           | 1,2 | 0,465     | 21,0        | LOS C            | 2,2               | 15,3     | 0,94      | 1,33           | 2,78                | 53,5        |
| Approach                     |      |           | 200          | 1,2 | 200           | 1,2 | 0,465     | 21,3        | LOS C            | 2,2               | 15,3     | 0,94      | 1,33           | 2,78                | 53,5        |
| All Vehicles                 |      |           | 909          | 1,3 | 909           | 1,3 | 0,568     | 17,1        | LOS C            | 3,0               | 21,3     | 0,84      | 1,38           | 2,81                | 52,1        |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab).  
 Vehicle movement LOS values are based on average delay per movement.  
 Intersection and Approach LOS values are based on average delay for all vehicle movements.  
 Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).  
 Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Gap.  
 HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.  
 Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

# NETWORK SUMMARY

■ Network: N101 [2028 + Dev AM (Network Folder: 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)

| Network Performance - Hourly Values  |           |         |                  |
|--------------------------------------|-----------|---------|------------------|
| Performance Measure                  | Vehicles: | All MCs | Persons          |
| Network Level of Service (LOS)       |           | LOS B   |                  |
| Speed Efficiency                     |           | 0,84    |                  |
| Travel Time Index                    |           | 8,27    |                  |
| Congestion Coefficient               |           | 1,18    |                  |
| Travel Speed (Average)               | km/h      | 50,7    | 50,7 km/h        |
| Travel Distance (Total)              | veh-km/h  | 1829,7  | 2195,7 pers-km/h |
| Travel Time (Total)                  | veh-h/h   | 36,1    | 43,3 pers-h/h    |
| Desired Speed                        | km/h      | 60,0    |                  |
| Demand Flows (Total for all Sites)   | veh/h     | 1282    | 1539 pers/h      |
| Arrival Flows (Total for all Sites)  | veh/h     | 1282    | 1539 pers/h      |
| Demand Flows (Entry Total)           | veh/h     | 963     |                  |
| Midblock Inflows (Total)             | veh/h     | 231     |                  |
| Midblock Outflows (Total)            | veh/h     | -153    |                  |
| Percent Heavy Vehicles (Demand)      | %         | 1,8     |                  |
| Percent Heavy Vehicles (Arrival)     | %         | 1,8     |                  |
| Degree of Saturation                 |           | 0,598   |                  |
| Control Delay (Total)                | veh-h/h   | 5,51    | 6,62 pers-h/h    |
| Control Delay (Average)              | sec       | 15,5    | 15,5 sec         |
| Control Delay (Worst Lane by MC)     | sec       | 22,8    |                  |
| Control Delay (Worst Movement by MC) | sec       | 26,8    | 26,8 sec         |
| Geometric Delay (Average)            | sec       | 6,3     |                  |
| Stop-Line Delay (Average)            | sec       | 9,2     |                  |
| Ave. Que Storage Ratio (Worst Lane)  |           | 0,03    |                  |
| Effective Stops (Total)              | veh/h     | 1441    | 1729 pers/h      |
| Effective Stop Rate                  |           | 1,12    | 1,12             |
| Proportion Queued                    |           | 0,70    | 0,70             |
| Performance Index                    |           | 62,6    | 62,6             |
| Cost (Total) *                       | \$/h      | 1642,27 | 1642,27 \$/h     |
| Fuel Consumption (Total)             | L/h       | 146,0   |                  |
| Fuel Economy                         | L/100km   | 8,0     |                  |
| Carbon Dioxide (Total)               | kg/h      | 344,3   |                  |
| Hydrocarbons (Total)                 | kg/h      | 0,028   |                  |
| Carbon Monoxide (Total)              | kg/h      | 0,41    |                  |
| NOx (Total)                          | kg/h      | 0,305   |                  |

Network Model Variability Index (Average value of largest changes in Lane Degrees of Saturation or Queue Storage Ratios from the third to the last Network Iterations): 0,0 %

Number of Iterations: 5 (Maximum: 30)

Largest change in Lane Degrees of Saturation or Queue Storage Ratios for the last three Network Iterations: 0,0% 0,0% 0,0%

Network Level of Service (LOS) Method: SIDRA Speed Efficiency.

Software Setup used: Standard Left.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

| Network Performance - Annual Values |           |         |                     |
|-------------------------------------|-----------|---------|---------------------|
| Performance Measure                 | Vehicles: | All MCs | Persons             |
| Demand Flows (Total for all Sites)  | veh/y     | 615 411 | 738 493 pers/y      |
| Delay (Total)                       | veh-h/y   | 2 647   | 3 177 pers-h/y      |
| Effective Stops (Total)             | veh/y     | 691 488 | 829 786 pers/y      |
| Travel Distance (Total)             | veh-km/y  | 878 262 | 1 053 915 pers-km/y |
| Travel Time (Total)                 | veh-h/y   | 17 336  | 20 803 pers-h/y     |
| Cost (Total)                        | \$/y      | 788 290 | 788 290 \$/y        |
| Fuel Consumption (Total)            | L/y       | 70 064  |                     |

|                         |      |         |
|-------------------------|------|---------|
| Carbon Dioxide (Total)  | kg/y | 165 265 |
| Hydrocarbons (Total)    | kg/y | 14      |
| Carbon Monoxide (Total) | kg/y | 195     |
| NOx (Total)             | kg/y | 146     |

1 Hours per Year: 480 (Network)

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# LEVEL OF SERVICE

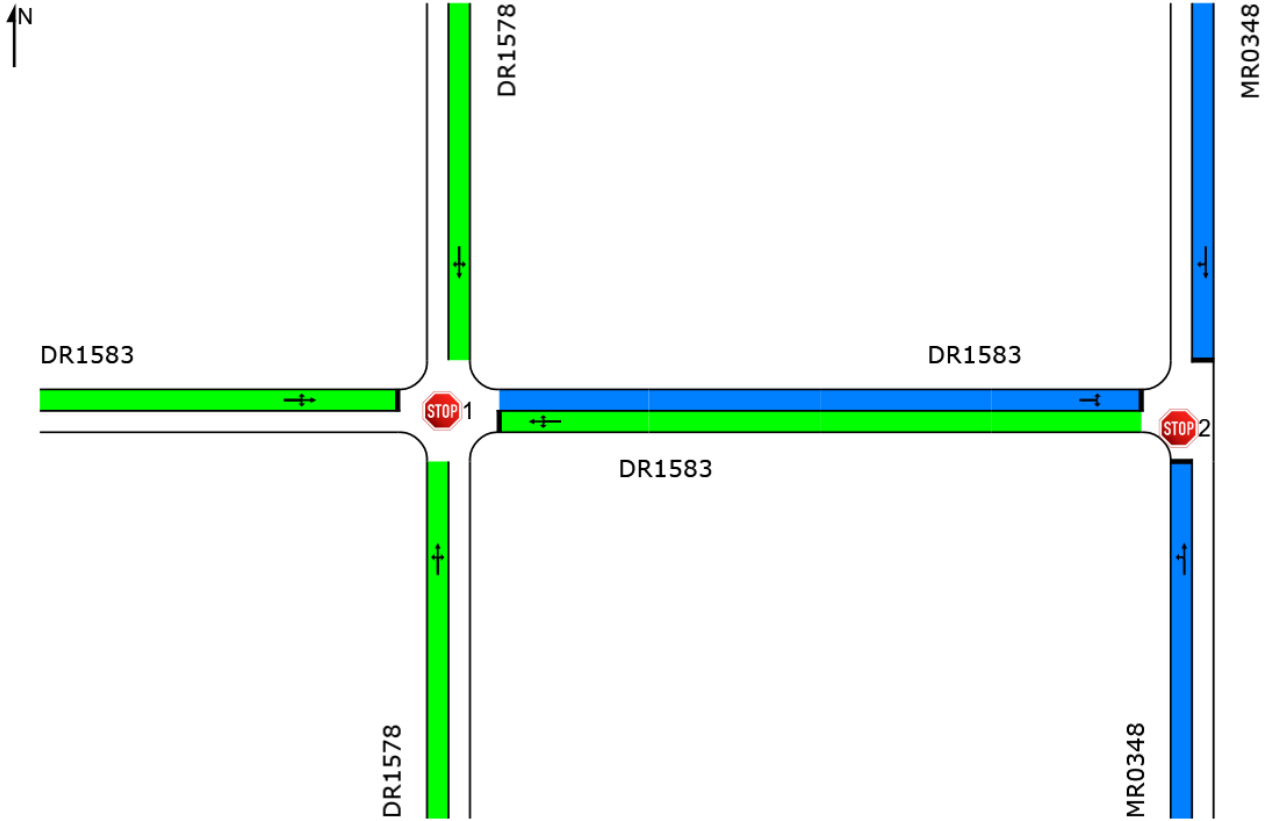
Lane Level of Service

■ Network: N101 [2028 + Dev AM (Network Folder: 2028 + Dev)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)



Colour code based on Level of Service



Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

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# NETWORK SUMMARY

■ Network: N101 [2028 AM (Network Folder: 2028)]

Output produced by SIDRA INTERSECTION Version: 9.1.3.210

New Network

Network Category: (None)

| Network Performance - Hourly Values  |           |         |                  |
|--------------------------------------|-----------|---------|------------------|
| Performance Measure                  | Vehicles: | All MCs | Persons          |
| Network Level of Service (LOS)       |           | LOS B   |                  |
| Speed Efficiency                     |           | 0,85    |                  |
| Travel Time Index                    |           | 8,31    |                  |
| Congestion Coefficient               |           | 1,18    |                  |
| Travel Speed (Average)               | km/h      | 50,9    | 50,9 km/h        |
| Travel Distance (Total)              | veh-km/h  | 1727,0  | 2072,5 pers-km/h |
| Travel Time (Total)                  | veh-h/h   | 34,0    | 40,7 pers-h/h    |
| Desired Speed                        | km/h      | 60,0    |                  |
| Demand Flows (Total for all Sites)   | veh/h     | 1239    | 1487 pers/h      |
| Arrival Flows (Total for all Sites)  | veh/h     | 1239    | 1487 pers/h      |
| Demand Flows (Entry Total)           | veh/h     | 952     |                  |
| Midblock Inflows (Total)             | veh/h     | 207     |                  |
| Midblock Outflows (Total)            | veh/h     | -149    |                  |
| Percent Heavy Vehicles (Demand)      | %         | 1,9     |                  |
| Percent Heavy Vehicles (Arrival)     | %         | 1,9     |                  |
| Degree of Saturation                 |           | 0,570   |                  |
| Control Delay (Total)                | veh-h/h   | 5,07    | 6,08 pers-h/h    |
| Control Delay (Average)              | sec       | 14,7    | 14,7 sec         |
| Control Delay (Worst Lane by MC)     | sec       | 22,2    |                  |
| Control Delay (Worst Movement by MC) | sec       | 26,3    | 26,3 sec         |
| Geometric Delay (Average)            | sec       | 6,2     |                  |
| Stop-Line Delay (Average)            | sec       | 8,5     |                  |
| Ave. Que Storage Ratio (Worst Lane)  |           | 0,03    |                  |
| Effective Stops (Total)              | veh/h     | 1362    | 1634 pers/h      |
| Effective Stop Rate                  |           | 1,10    | 1,10             |
| Proportion Queued                    |           | 0,69    | 0,69             |
| Performance Index                    |           | 58,4    | 58,4             |
| Cost (Total) *                       | \$/h      | 1546,75 | 1546,75 \$/h     |
| Fuel Consumption (Total)             | L/h       | 138,2   |                  |
| Fuel Economy                         | L/100km   | 8,0     |                  |
| Carbon Dioxide (Total)               | kg/h      | 326,0   |                  |
| Hydrocarbons (Total)                 | kg/h      | 0,027   |                  |
| Carbon Monoxide (Total)              | kg/h      | 0,38    |                  |
| NOx (Total)                          | kg/h      | 0,294   |                  |

Network Model Variability Index (Average value of largest changes in Lane Degrees of Saturation or Queue Storage Ratios from the third to the last Network Iterations): 0,0 %

Number of Iterations: 5 (Maximum: 30)

Largest change in Lane Degrees of Saturation or Queue Storage Ratios for the last three Network Iterations: 0,0% 0,0% 0,0%

Network Level of Service (LOS) Method: SIDRA Speed Efficiency.

Software Setup used: Standard Left.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

| Network Performance - Annual Values |           |         |                   |
|-------------------------------------|-----------|---------|-------------------|
| Performance Measure                 | Vehicles: | All MCs | Persons           |
| Demand Flows (Total for all Sites)  | veh/y     | 594 695 | 713 634 pers/y    |
| Delay (Total)                       | veh-h/y   | 2 433   | 2 919 pers-h/y    |
| Effective Stops (Total)             | veh/y     | 653 702 | 784 442 pers/y    |
| Travel Distance (Total)             | veh-km/y  | 828 983 | 994 780 pers-km/y |
| Travel Time (Total)                 | veh-h/y   | 16 300  | 19 560 pers-h/y   |
| Cost (Total)                        | \$/y      | 742 442 | 742 442 \$/y      |
| Fuel Consumption (Total)            | L/y       | 66 340  |                   |

|                         |      |         |
|-------------------------|------|---------|
| Carbon Dioxide (Total)  | kg/y | 156 501 |
| Hydrocarbons (Total)    | kg/y | 13      |
| Carbon Monoxide (Total) | kg/y | 184     |
| NOx (Total)             | kg/y | 141     |

1 Hours per Year: 480 (Network)

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